Tritax Symmetry (Hinckley) Limited

HINCKLEY NATIONAL RAIL FREIGHT INTERCHANGE

The Hinckley National Rail Freight Interchange Development Consent Order

Project reference TR050007

Environmental Statement Volume 2: Appendices

Appendix 8.1: Transport Assessment (part 9 of 20) Furnessing Methodology

Document reference: 6.2.8.1

Revision: 07

September 2023

Planning Act 2008

The Infrastructure Planning (Applications: Prescribed Forms and Procedure) Regulations 2009 Regulation 5(2)(a)

The Infrastructure Planning (Environmental Impact Assessment) Regulations 2017 Regulation 14

This document forms a part of the Environmental Statement for the Hinckley National Rail Freight Interchange project.

Tritax Symmetry (Hinckley) Limited (TSH) has applied to the Secretary of State for Transport for a Development Consent Order (DCO) for the Hinckley National Rail Freight Interchange (HNRFI).

To help inform the determination of the DCO application, TSH has undertaken an environmental impact assessment (EIA) of its proposals. EIA is a process that aims to improve the environmental design of a development proposal, and to provide the decision maker with sufficient information about the environmental effects of the project to make a decision.

The findings of an EIA are described in a written report known as an Environmental Statement (ES). An ES provides environmental information about the scheme, including a description of the development, its predicted environmental effects and the measures proposed to ameliorate any adverse effects.

Further details about the proposed Hinckley National Rail Freight Interchange are available on the project website:

http://www.hinckleynrfi.co.uk/

The DCO application and documents relating to the examination of the proposed development can be viewed on the Planning Inspectorate's National Infrastructure Planning website:

https://infrastructure.planninginspectorate.gov.uk/projects/east-midlands/hinckley-national-rail-freight-interchange/



TRANSPORT & INFRASTRUCTURE PLANNING

Tritax Symmetry Ltd Hinckley National Rail Freight Interchange Furnessing Methodology



TRANSPORT & INFRASTRUCTURE PLANNING

Tritax Symmetry Ltd Hinckley National Rail Freight Interchange Furnessing Methodology

> Birmingham Livery Place, 35 Livery Street, Colmore Business District Birmingham, B3 2PB T: 0121 233 3322

> > Whitehall Waterfront, 2 Riverside Way Leeds, LS1 4EH T: 0113 233 8000

> > > London 11 Borough High Street London, SE1 9SE T: 0207 407 3879

Manchester 11 Portland Street Manchester, M1 3HU T: 0161 233 4260

Market Harborough Harborough Innovation Centre, Wellington Way, Airfield Business Park, Leicester Road Market Harborough, Leicestershire, LE16 7WB T: 01858 455020

> Nottingham 5th Floor, Waterfront House, Station Street Nottingham, NG2 3DQ T: 0115 924 1100

> > September 2023



DOCUMENT ISSUE RECORD

Document Number:	HNRFI-BWB-GEN-XX-RP-TR-0022-S4-P03_Furnessing Methodology
BWB Reference:	NTT2814

Revision	Date of Issue	Status	Author:	Checked:	Approved:
1	07/07/21	\$4	Vibeeshan Devaharan	Malcolm Ash	Shirley Dumigan
2	27/04/22	\$4	Vibeeshan Devaharan	Malcolm Ash	
3	01/08/22	\$4	Vibeeshan Devaharan	Malcolm Ash	
4	04/09/23	\$4	Vibeeshan Devaharan	Malcolm Ash	

Notice

This document has been prepared for the sole use of the Client in accordance with the terms of the appointment under which it was produced. BWB Consulting Limited accepts no responsibility for any use of or reliance on the contents of this document by any third party. No part of this document shall be copied or reproduced in any form without the prior written permission of BWB.



CONTENTS

1.	INTRODUCTION	. 4
2.	BACKGROUND	. 4
3.	DETAILED FURNESS METHODOLOGY	. 5
4.	SITE ACCESS JUNCTIONS	. 6
5.	SUMMARY	. 7

FIGURES

Figure 1: Option 3 Furnessing Methodology Figure 2: Revised Furnessing Methodology Figure 3: Site Access Furnessing Methodology

APPENDICES

Appendix A: Hydrock Furnessing Technical Note

Appendix B: LCC Correspondence



1. INTRODUCTION

- 1.1 BWB Consulting has been commissioned as part a wider project scope by Tritax Symmetry Ltd to develop a series of highway models capable of assessing highway impacts from the proposed Hinckley National Rail Freight Interchange (HNRFI) development. The site will be developed to serve a maximum of 850,000sqm of B8 warehousing/distribution uses and a rail freight terminal.
- 1.2 A strategic model PRTM V1.0 was utilised initially to undertake modelling of future forecast scenarios. At the request of the HNRFI Transport Working Group (TWG) and specifically Leicestershire County Council, an updated version of the model has been used (PRTM V2.2) which includes for more detailed trip generation of committed schemes as well as committed infrastructure within the modelling extent.
- 1.3 This note has been produced to detail the furnessing methodology undertaken to derive future forecast traffic flow matrices for junctions assessed.

2. BACKGROUND

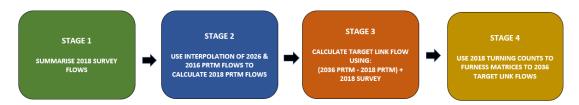
- 2.1 Hydrock previously produced a technical note (07700-HYD-XX-XX-RP-TP-1021 Rev. P02) which detailed three different methodologies of furnessing the PRTM data. A copy of the technical note is provided in **Appendix A**. A short summary of each option has been provided below.
 - **Option 1**: Use target entry and exit flows directly extracted from PRTM;
 - **Option 2**: Use linear interpolation to obtain 2018 PRTM base and use this in conjunction with future PRTM flows to derive growth factors. These growth rates are then applied to observed flows to derive future forecast flows and junctions; and
 - **Option 3:** Use linear interpolation to obtain 2018 PRTM base and calculate absolute differences in link flows between calculated 2018 PRTM and the respective future year PRTM flows. The absolute differences are then added to 2018 observed flows to derive future forecast link flows for each scenario. The base 2018 observed turning counts are then used to furness the future forecast matrices.
- 2.2 Following the submission of the options above by Hydrock, LCC considered Option 3 as the preferable option, and this was agreed in November 2019. A copy of the correspondence is provided in **Appendix B**.
- 2.3 BWB has also reviewed the methodologies and compared the multiplicative (Option 2) and additive (Option 3) approaches proposed in the options for furnessing. It was considered that the multiplicative approach could provide growth factors too great a variance which subsequently may provide unrealistic forecast traffic flows at junctions. Option 3 which is the Interpolation and Application of Absolute Growth is considered more appropriate, which will use PRTM flows to calculate absolute changes in flows and assume the reassignment of traffic forecast in PRTM is correct as opposed to the flows directly extracted from PRTM. Based on this, BWB considers Option 3 the preferable and acceptable furnessing methodology, and this has been utilised to furness traffic flow matrices.



3. **DETAILED FURNESS METHODOLOGY**

3.1 Option 3 of the furnessing methodologies had been utilised to furness the traffic flow matrices at the junctions of interest. A flow chart of the methodology is provided in Figure 1 below.

Figure 1: Option 3 Furnessing Methodology



3.2 However the PRTM 2.2 SATURN outputs provided a 2019 traffic flow scenario therefore, instead of interpolating between PRTM 2016 and 2026 to obtain a 2018 PRTM base flows, it is considered that Stage 2 to is altered to growth 2018 survey flows using TEMPro to 2019 to derive an equivalent base year as PRTM. This provides a more robust basis for the furnessing as no further assumptions have to be made to derive a base flow scenario from PRTM, i.e. linear growth between PRTM scenarios. A revised flow chart of the methodology is presented in Figure 2 below.

Figure 2: Revised Furnessing Methodology



- 3.3 The furnessing methodology has been undertaken for each scenario separately, this includes 'Without Development', 'Without Development with Infrastructure' and 'With development with Infrastructure' for the years 2026 and 2036 respectively.
- 3.4 The furnessing has been built using an MS Excel macro using VBA to ensure an extensive spreadsheet is not required to display every iteration of the furnessing. This also ensures that the methodology is consistent between all furnessed matrices. A summary of the process undertaken by the macros is provided below.
 - 1. Column: adjustment: Calculate turning counts across column using survey data proportions in combination with the target link flow out of each arm
 - 2. Sum Row: Calculate the sum of each arm row total
 - 3. Row Adjustment: Calculate turning counts across rows using survey data proportions in combination with the target link flow into each arm
 - 4. Sum Column: Calculate sum of each column
 - 5. Round all values in matrix to the closest integer
 - 6. Update sums for column and row total
 - 7. Repeat the above 'x' number of iterations



- 3.5 The macro has been built to run the furnessing 20 times for each matrix, however it should be noted that every time the macro is executed, it runs an additional 20 times. The furnessing spreadsheet therefore has been run for at least 20 iterations. The furnessing methodology has been double constrained, i.e. both origin and destination and the traffic flow matrices are furnessed until link flows are within 2% of calculated link flows. This has been calculated by taking the absolute difference between the calculated target link flow and furnessed link flow. Should these be higher than 2%, the macro is executed until convergence is achieved.
- 3.6 Additional matrices are provided to calculate the absolute difference and percentage difference between the forecast and furnessed link flows for each scenario respectively. A review of these indicates that this is considered to be convergent with the accepted furnessing methodology.
- 3.7 Furnessing of traffic flow matrices based on the above methodology was initially undertaken using PRTM V1.0 data, HE and LCC reviewed the submitted information and broadly agreed with the calculation. However, HE has queried the negative growth applied at some junctions and queried whether negative growth should be excluded as part of furnessing.
- 3.8 PRTM model was utilised for the scheme to understand what the reassignment of traffic is due to the proposed scheme and infrastructure. PRTM reassigns vehicle routes based on delays and cost of journey therefore some movements may experience reduction in flows whilst some increase which is considered acceptable as the model was built to illustrate the changes and impact of flows on junctions.
- 3.9 Furthermore, PRTM V1.0 has been revised with more detailed trip generation of committed developments and also includes revised committed infrastructure improvements. Excluding negative growth would overestimate impacts at junctions therefore, it is considered that PRTM V2.2 should be acceptable to understand what the reassignment of traffic is within the modelling extent.

4. SITE ACCESS JUNCTIONS

- 4.1 M69 Junction 2 provides access into the proposed site. Furthermore, as part of the access strategy, south facing on and off slip roads are proposed at M69 Junction 2.
- 4.2 The agreed furnessing methodology utilises the observed turning movements in combination with calculated forecast link flows to furness future year flow matrices. However, it is considered that this approach is not applicable to M69 Junction 2 as three additional arms are added to the junction and as these do not have any base flows, furnessing cannot be undertaken.
- 4.3 Furthermore, the proposed scheme will significantly alter the movement at the junction with rerouting of traffic through the junction, therefore it is proposed that a different approach for 'Stage 4' is taken only for the site access junctions. Instead of using observed turning count proportions to furness the matrices, we will use the PRTM turning counts for the respective future year scenarios as a prior matrix to furness the matrices. This methodology utilises observed counts to calculate a more realistic link flow target at the junction whilst accounting for the redistribution of traffic anticipated at M69 J2



with the inclusion of new arms to the junction. Similar approach would be taken for the secondary access. Please see revised methodology for site access junctions below.

Figure 3: Site Access Furnessing Methodology



- 4.4 A VISSIM model of M69 J2 was obtained from National Highways and recalibrated to provide a basis for future year assessment. The model utilises static routing assignment therefore the furnessed matrices will be directly input into the model to derive the future year scenarios.
- 4.5 Further to the above, junctions along the proposed spine road utilise a first principles method to derive forecast traffic flow matrices for junction capacity assessments. The spine road movements are extracted from PRTM for the respective scenarios and development traffic from minor arms will be calculated utilising agreed trip distribution.

SUMMARY

- 5.1 PRTM V1.0 has been revised to PRTM V2.2 to include for more detailed trip generation of committed schemes as well as include for committed schemes within the modelling extent.
- 5.2 As part of PRTM V1.0, it was agreed that Option 3 of the furnessing methodologies presented was the most preferable option. This utilises interpolation of PRTM flows to derive a common base year with observed data and calculate absolute differences in links flows between calculate PRTM base flows and subsequent future year scenarios to provide forecast link flows. Subsequently these are furnessed using turning count proportions from observed data to derive future year flow matrices.
- 5.3 The furnessing methodology is applied to all junctions with the exception of M69 Junction 2, the proposed second access on the B4668 Leicester Road. As there are additional arms to these junctions, it is considered more appropriate to use the respective PRTM future year turning proportions to furness the matrices. Furthermore, proposed junctions along the spine road will utilise a first principles method to calculate forecast traffic matrices.





Project name	Hinckley National Rail Freight Interchange						
Design note title	Furness Modelling Methodology						
Document reference	07770-HYD-XX-XX-RP-TP-1021						
Author	Vassil Pavlov						
Checker/Approver	Luke Hutcheson/Rory McHugh						
Revision	P01						
Date	9 August 2019 Approved ✓						

1. INTRODUCTION

1.1 Preamble

- 1.1.1 This Technical Note [TN] has been prepared with the aim of summarising the application of the Furness method to observed traffic flows and setting out the chosen methodology, giving justification for its validity and suitability as well as the appropriateness of the adopted approach, particularly with regards to convergence and intended outcomes.
- 1.1.2 The exercise is undertaken as part of the wider transport modelling methodology for the Hinckley National Rail Freight Interchange [NRFI]. It forms the backbone of the more detailed junction capacity modelling, to be carried out in subsequent stages of the analysis.

1.2 Modelling Context

- 1.2.1 The method follows on from the outputs of the Pan Regional Transport Model [PRTM], with the modelling results presented in the AECOM report "PRTM Hinckley NRFI Application: Forecast Modelling v1.0" and the subsequent filtering process undertaken by Hydrock, presented in the technical note "Strategic Traffic Modelling Results An Interim Summary".
- 1.2.2 The use of the PRTM and the methodology for undertaking the strategic modelling has been agreed previously and is not discussed further here.
- 1.2.3 Various assessment scenarios have been/will be modelled using the PRTM, with the results being presented in various output files in the form of image plots, excel files and MapInfo formats for total vehicle flows and splits for light vehicles and HGVs.
- 1.2.4 The performed primary and secondary filtering process has significantly reduced the total number of nodes to 63, with a VoC in excess of 85% in any assessment scenario and a development impact of +/- 5% defined as critical thresholds. Further consultation with the relevant LHAs established an additional performance indicator of +30 vehicles impact. This was deemed appropriate to overcome spurious values of VoC resulting from modelling noise. The final number of junctions agreed for further analysis is still to be agreed, with local factors/judgement to be applied.
- 1.2.5 The Furness procedure outlined in this note facilitates the transition from strategic to local junction modelling in an attempt to derive a future year origin-destination (entry-exit) matrix for each junction



assessed. Moreover, the process is used to further gauge the change in traffic flows and inform the need for detailed capacity assessments.

PROPOSED METHODOLOGY

2.1 Purpose of Furness Procedure

- 2.1.1 The strategic modelling outputs are presented in the form of link flows. These form the target entry and exit trip ends for each junction in the future assessment years of 2026 and 2036 i.e. the total number of vehicles to and from each arm.
- 2.1.2 The link flows for the Base scenario in all assessment years are contained in **Appendix A**. The node references used to define the individual links can be located at:
- 2.1.3 In order to derive a future year matrix that respects the forecast trip ends, a method of bi-proportional adjustment, also known as the Furness method, is followed. The Furness method, typically having applications in strategic modelling as a trip distribution tool, achieves a doubly constrained solution through successive factoring of individual matrix entries, thus reconciling an observed base matrix with both sets of forecast trip ends.
- 2.1.4 The method relies on the assumption that the pattern of travel in the future year will remain substantially identical, with traffic increasing in line with individual entry/exit growth. Different sets of growth factors are, therefore, applied to each column and row entry until convergence is reached. The doubly constrained solution is achieved when the derived matrix is adjusted accordingly and respects the forecasted trip ends.
- 2.1.5 The incremental steps taken to perform the procedure are more thoroughly scrutinised in the following sections, where the New Road/Long Street/Broughton Road junction is used as an illustrative example.
- 2.1.6 The mathematical notation used throughout this report is explained in **Appendix B**.

2.2 Traffic Survey Data and Base Matrix

- 2.2.1 Manual Classified Turning Count surveys were commissioned in 2018/2019 for all junctions potentially requiring a more detailed review. The raw survey data for the example junction discussed here (New Road/Long Street/Broughton Road) is provided in **Appendix C** for reference.
- 2.2.2 To ensure consistency with the PRTM outputs, the data was processed to yield the turning movements at the junction for the modelled AM and PM peak hours of 08:00 09:00 and 17:00 18:00 respectively. The resulting 2018 Origin-Destination [O-D] Base Matrices (in veh/hr) as derived from the traffic surveys are illustrated in Table 2.1 and Table 2.2.

Table 2.1: 2018 Base Matrix AM (Veh/hr)

From\To	Α	В	С	D	Total
Α	0	62	79	209	350
В	33	0	12	242	287
С	41	4	1	75	121
D	155	337	118	0	610
Total	229	403	210	526	1368



Table 2.2: 2018 Base Matrix PM (Veh/hr)

From\To	А	В	С	D	Total
А	0	56	70	152	278
В	69	0	8	377	454
С	78	7	1	143	229
D	225	286	116	0	627
Total	372	349	195	672	1588

2.3 Forecast Trip Ends

2.3.1 As already mentioned, the purpose of the Furness method is to adjust the base matrix to match the forecast trip ends (i.e. row and column totals) for the future year scenarios. To achieve this, two variations of the method are proposed to be followed.

Option 1 - Extraction of Target Trip Ends Directly from PRTM

- 2.3.2 The first method involves taking the forecast link flows directly from the PRTM and using those as the target entry and exit flows for each arm.
- 2.3.3 The advantage of this method is the ensured consistency with the wider assessment methodology and reduced number of assumptions applied to derive the target trip ends. Additionally, the flow assignment in this set of forecasts fully takes into account the available capacity within the network, thus ensuring that no unrealistic volumes are being assigned.
- 2.3.4 However, following detailed discussions with the AECOM modelling team, concerns were raised that such an approach could potentially place too much reliance on the forecast flows from the PRTM. Due to its strategic nature, only the base model of the PRTM is validated against observed data, albeit not calibrated/validated against individual turning movements.

Option 2 - Interpolation and Growth Factoring of Trip Ends

2.3.5 A second method giving more confidence in the growth predicted by the model is also considered. The approach involves using the 2016 and 2026 Base scenarios and interpolation to obtain the 2018 flow for each target entry and exit link flow. A linear interpolation formula is used to derive the 2018 values. The equations are shown below for both origins and destinations:

$$Q_{i_{2018}} = \frac{(2018 - 2016)(Q_{i_{2026}} - Q_{i_{2016}})}{(2026 - 2016)} + Q_{i_{2016}}$$

$$Q_{j_{2018}} = \frac{(2018 - 2016)(Q_{j_{2026}} - Q_{j_{2016}})}{(2026 - 2016)} + Q_{j_{2016}}$$

- 2.3.6 The forecast change in flows to 2036 has then been used to obtain appropriate growth factors that have in turn been used to multiply the observed (base 2018) trip ends. This generates target row and column totals which utilise both the base matrix and the growth predicted by the model and eliminates discrepancies between the two data sources.
- 2.3.7 However, a disadvantage of this method is the potential for artificially inflated flows which are not representative of the future conditions. As such, they would in some instances be reassigned by the



model due to an increased congestion factor. It is also worth noting that in the PRTM only a portion of the growth determines the forecast while the rest of it is the function of the future year forecast itself. Therefore, such an approach could lead to inaccurate results.

2.4 Trip End Balancing

2.4.1 The second method creates the need for trip end balancing due to the disproportionate increase/reduction for each set of targets. A common method of balancing trip ends is to balance destinations with respect to origins on the assumption that those are considered more reliable in terms of correctness. However, in order to recognise the validity of both sets of trip ends, the average of the two is taken and the rows and columns balanced to match the said average. The implementation of this step is mathematically formulated below:

$$T_{Av} = \frac{\sum_{ij} (X_i + Y_j)}{2}$$

$$O_i = X_i \frac{T_{Av}}{\sum_i X_i}$$

$$D_j = Y_j \frac{T_{Av}}{\sum_i Y_i}$$

2.5 Method Comparison

2.5.1 The two methods have been carried out as described. The following forecast trip ends are hence derived for both the AM and PM conditions. These are presented alongside the base matrix to aid reader comprehension of the methods. Table 2.3 through to Table 2.6 illustrate.

Table 2.3: Method 1 - Target Trip Ends from PRTM - AM (Veh/hr)

From\To	Α	В	С	D	Total	Target
Α	0	62	79	209	350	152
В	33	0	12	242	287	395
С	41	4	1	75	121	160
D	155	337	118	0	610	742
Total	229	403	210	526	1368	
Target	114	389	330	617		

Table 2.4: Method 1 - Target Trip Ends from PRTM - PM (Veh/hr)

From\To	Α	В	С	D	Total	Target
Α	0	56	70	152	278	238
В	69	0	8	377	454	372
С	78	7	1	143	229	447
D	225	286	116	0	627	685
Total	372	349	195	672	1588	
Target	571	281	159	732		



Table 2.5: Method 2 - Balanced Forecast Trip Ends - AM (Veh/hr)

From\To	Α	В	С	D	Total	Target
Α	0	62	79	209	350	538
В	33	0	12	242	287	261
С	41	4	1	75	121	111
D	155	337	118	0	610	634
Total	229	403	210	526	1368	
Target	223	450	321	548		1543

Table 2.6: Method 2 - Balanced Forecast Trip Ends - PM (Veh/hr)

From\To	Α	В	С	D	Total	Target
Α	0	56	70	152	278	268
В	69	0	8	377	454	560
С	78	7	1	143	229	243
D	225	286	116	0	627	679
Total	372	349	195	672	1588	
Target	515	340	190	706		1751

- 2.5.2 The two sets of forecasts are compared to establish if there are significant differences between them. If the difference is shown to be immaterial, the preference is to proceed using the calibrated and validated PRTM flows. This also ensures consistency with the wider scoping and filtering methodology undertaken to date.
- 2.5.3 If significant discrepancies are identified on one or more links, this will be evaluated to determine the most appropriate method to follow. If deemed necessary the interpolated and factored targets will be used to carry out the Furness procedure. Conversely, if there is sufficient evidence to suggest that the PRTM forecast yields a more realistic representation of the future year conditions, then the same method will be followed as before.
- 2.5.4 Table 2.7 and Table 2.8 illustrate the differences between the two alternatives.

Table 2.7: Forecast Difference AM

Arm		Row Totals			Column Totals	
	Method 1	Method 2	Difference	Method 1	Method 2	Difference
Α	152	538	+386	114	223	+109
В	395	261	-134	389	450	+61
С	160	111	-49	330	321	-9
D	742	634	-108	617	548	-69

Table 2.8: Forecast Difference PM

Arm		Row Totals			Column Totals	
	Method 1	Method 2	Difference	Method 1	Method 2	Difference
Α	238	268	+30	571	515	-56
В	372	560	+188	281	340	+59
С	447	243	-204	159	190	+31
D	685	679	-6	732	706	-26



- 2.5.5 From the tables it is evident that there are significant differences between the two sets of forecasts. For the purpose of this TN it is proposed that the flows taken directly from the PRTM forecast are used to perform the Furness procedure at the Road/Long Street/Broughton Road junction.
- 2.5.6 However, it is worth noting that this position is not final and Hydrock are currently in the process of performing further spot checks and sensitivity tests at four additional junctions in order to establish the validity of the PRTM base model when compared directly against the observed 2018/2019 base. The GEH Statistic has been used to gauge whether there is a statistically significant difference between the two and the output will be used to further inform a decision on the most appropriate set of forecast flows to be used in the Furness procedure.

2.6 Iterative Process

- 2.6.1 With the base matrix and balanced forecast trip ends now confirmed, the iterative process of biproportional adjustment can begin. The process is divided into iterations, with each consisting of factor
 derivation and the subsequent adjustment of the base matrix in the order to derive the individual
 entries in the future year O-D matrix, respecting both sets of target trip ends. Each iteration consists of
 five stages, described as followed:
 - 1. Calculation of column factors
 - 2. Adjustment of column entries by the calculated factors
 - 3. Calculation of row factors
 - 4. Adjustment of row entries by the calculated factors
 - 5. Rounding of Matrix Entries
- 2.6.2 The column and row factors are calculated by dividing the target trip end by the sum of the individual entries in the column or row. This is illustrated below.

$$r_i = \frac{O_i}{\sum_j B_{ij}}$$

$$c_j = \frac{D_j}{\sum_i B_{ij}}$$

2.6.3 The derived factors are then applied in succession. The column factors are applied to the base matrix, while the row factors are then applied to the resulting, partially adjusted matrix. The two steps are summarised below:

$$R_{ij} = c_j B_{ij}$$

$$I_{ij} = rR_{ij}$$

- 2.6.4 At the end of the first iteration the resulting matrix is described as an intermediate matrix, according with the trip-ends used to obtain the second set of factors but not the first. At this stage a singly constrained solution is reached.
- 2.6.5 In order to reconcile the matrix with both sets of trip ends, the process is continued until both sets are matched and a doubly constrained solution is accomplished. This entails further iterations of the same nature. With each successive iteration the sum of the individual entries will get closer to their respective targets and will thus near convergence. This is reflected in the calculated factors which will approach 1.



2.7 Convergence Measure and Defined Criterion

2.7.1 At the end of each iteration, checks for convergence are performed to ensure row and column totals are within a permissible degree of unity with their target trip ends. For this exercise that threshold is set at 1%. The convergence criterion used is the Relative Absolute Difference [RAD], calculated as:

$$\left| \frac{\sum_{i} F_{kij} - D_{j}}{D_{i}} \right| \leq \varepsilon, \forall j$$

- 2.7.2 The RAD is calculated for all columns at the end of each iteration. No test for convergence is carried out for the row totals as this is the last parameter to be adjusted. Therefore, the sum of the individual matrix entries will equal the forecast target and the RAD will be 0.
- 2.7.3 The process is completed when the RAD for all columns is ≤ 1%. If the value of RAD is above the threshold on one or more columns the iterations continue until convergence is reached. The Furness method will almost always converge, often within a small number of iterations, provided that the trip ends are balanced.
- 2.7.4 The number of iterations has been set at 20, believing that to be sufficient for convergence to be achieved. The final adjusted matrices for the AM and PM peaks are shown in Table 2.9 and Table 2.10.

Table 2.9: Final 2036 Matrix AM (Veh/hr)

From\To	Α	В	С	D	Total
Α	0	15	30	107	152
В	11	0	17	367	395
С	17	4	2	137	160
D	87	372	283	0	742
Total	115	391	332	611	1449

Table 2.10: Final 2036 Matrix PM (Veh/hr)

From\To	Α	В	С	D	Total
Α	0	36	48	155	239
В	63	0	5	304	372
С	166	9	0	271	446
D	343	237	106	0	686
Total	572	282	159	730	1744

2.8 Application to HGV Flows

2.8.1 In order to use the output from the Furness method for detailed junction modelling purposes, the flows must be converted to PCUs. This can be achieved by estimating the future HGV flows, with the same procedure of bi-proportional adjustment followed. The base matrix along with the forecast row and column totals are shown in Table 2.11 and Table 2.12.



Table 2.11: 2018 Base Matrix and Forecast Trip Ends AM (HGVs)

From\To	Α	В	С	D	Total	Target
Α	0	3	0	2	5	1
В	1	0	0	17	18	11
С	2	0	0	5	7	8
D	0	18	1	0	19	19
Total	3	21	1	24	49	
Target	1	13	6	19		39

Table 2.12: 2018 Base Matrix and Forecast Trip Ends PM (HGVs)

From\To	Α	В	С	D	Total	Target
Α	0	1	1	2	4	1
В	1	0	0	18	19	8
С	1	0	0	3	4	8
D	3	9	2	0	14	10
Total	5	10	3	23	41	
Target	1	8	2	16		27

- 2.8.2 An issue that arises here is that for some junctions the HGV flows are very low, as a consequence of which the matrix entries for certain movements are displayed as 0. When there are too many zeros in the matrix the Furness method will fail to converge and may begin to diverge due to the continuous factoring of zeros.
- 2.8.3 At junctions where this is applicable, the problem has been overcome using a manual override. An IF statement has been inserted to detect where an imbalance exists in the final matrix in the range -1< >+1 and automatically reposition an HGV unit in the correct cell. Given the low numbers and the rounding performed at the end of each iteration, the RAD is displayed as 0 upon convergence.
- 2.8.4 The final adjusted HGV matrices are illustrated in Table 2.13 and Table 2.14.

Table 2.13: Final 2036 Matrix AM (HGVs/hr)

From\To	Α	В	С	D	Total
Α	0	0	0	1	1
В	0	0	0	11	11
С	1	0	0	7	8
D	0	13	6	0	19
Total	1	13	6	19	39

Table 2.14: Final 2036 Matrix PM (HGVs/hr)

From\To	Α	В	С	D	Total
Α	0	0	0	1	1
В	0	0	0	8	8
С	1	0	0	7	8
D	0	8	2	0	10
Total	1	8	2	16	26



CONCLUSION

3.1 Summary

3.1.1 The application of the Furness method has allowed for the number of trips to converge. While the second set of factoring effectively negates the convergence reached in the first, an intermediate solution is reached at the end of each cycle. The measure of convergence performed after each iteration is a check for this. The output from the exercise is the converged matrix which has been adjusted to respect the derived target trip ends. This has been obtained for both total vehicle traffic and HGVs at New Road/Long Street/Broughton Road.

3.2 General Remarks

- 3.2.1 The Furness method has been undertaken using two variations of the initial trip end derivation stage, namely (1) Direct extraction from PRTM and (2) Growth Interpolation. It should be appreciated that both identified methods have limitations and engineering judgement will be applied following conclusive results of the ongoing detailed review.
- 3.2.2 This methodology TN sets out the process of performing the Furness procedure, not the results. Following agreement to the process (which does not vary with year of assessment) the results will be provided for all of the relevant assessment years.

3.3 Next Steps

3.3.1 The next stage of the modelling process is to combine the total vehicle matrices with the HGV matrices for each junction in order to obtain the total flows in PCUs. An initial review will then be undertaken and engineering judgment applied to determine if detailed capacity modelling is justified. For all junctions where this is required, further assessments will be undertaken using the industry standard software packages Junctions 9 and LinSig 3. If capacity issues are experienced, mitigation designs will be prepared and agreed with the relevant LHAs.



Appendix A 'Base' and 'Base + New Slip Roads' Link Flows









Appendix B Mathematical Notation





i	Origin i
j	Destination j
Q _{iyear}	Flow from Arm i in particular modelled year
Q _{jyear}	Flow to Arm j in particular modelled year
Xi	Forecast Row Total for Arm i before balancing
Y_j	Forecast Column Total for Arm j before balancing
T_{Av}	Average Target Trip End Total
Oi	Forecast Row Total for Arm i after balancing
D_j	Forecast Column Total for Arm j after balancing
ri	Row Factor
Cj	Column Factor
B_{ij}	Entry in Base Matrix
R_{ij}	Entry in Resultant Matrix (after column factoring)
l _{ij}	Entry in Intermediate Matrix (end of iteration)
F_{kij}	Entry in Forecast Matrix for iteration k (when l_{ij} is converged)
ε	Convergence threshold
\mathbb{Z}_{j}	For All Destinations



Appendix C New Road/Long Street/Broughton Road Junction Raw Survey Data





Client: Hydrock

Project Number: TSP13881

Project Name: 07700 Hinckley NRFI

Survey Type: Manual Classified Turning Count

Survey Date: 26 Jun 2018, Tuesday

Survey Time: 07:00 - 19:00

Weather: Dry

Comments:

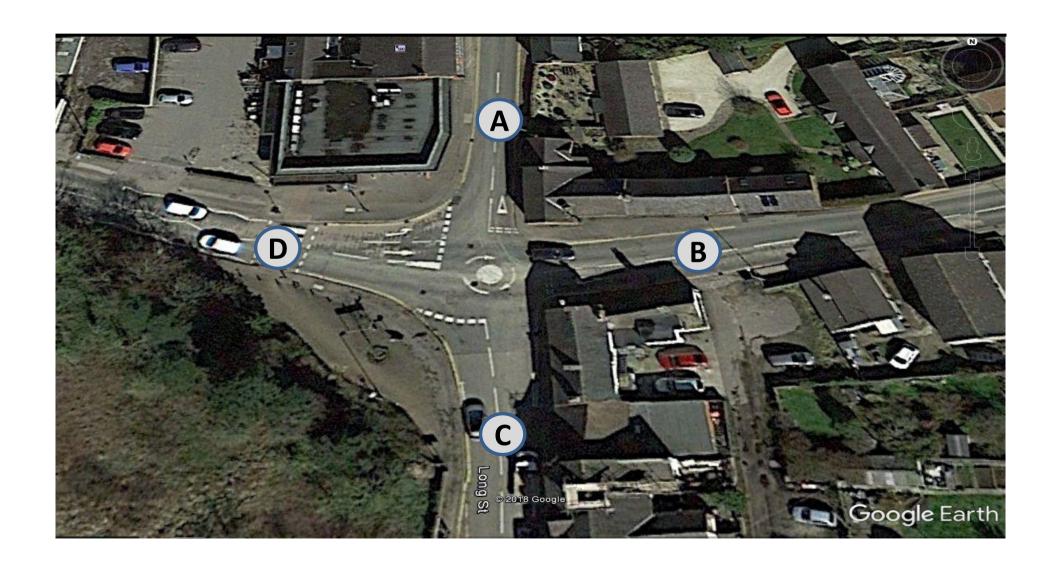
Project Name: 07700 Hinckley NRFI

Survey Type: Manual Classified Turning Count

Site No: 18

Location: New Road / Long Street / Broughton Road





Project Name: 07700 Hinckley NRFI
Survey Type: Manual Classified Turning Count

Site No: 18



	1	1	1.5	2.3	2 A ·	- A	0.4	0.2			A - B									
Time	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL
07:00									0	(PCU)	13	2		2					17	(PCU) 19.6
07:15									0	0	8	1	1						10	10.5
07:30 07:45									0	0	11 13	3							14 16	14 16
H/Total	0	0	0	0	0	0	0	0	0	0	45	9	1	2	0	0	0	0	57	60.1
08:00									0	0	14		_	_					14	14
08:15									0	0	20	2							22	22
08:30 08:45									0	0	10 10	1 2	1 1	1					13 13	14.8 13.5
H/Total	0	0	0	0	0	0	0	0	0	0	54	5	2	1	0	0	0	0	62	64.3
09:00									0	0	8	6							14	14
09:15 09:30	1								1 0	1 0	13 5		1						13 6	13 6.5
09:45									0	0	2	1	_	1		1		5	10	8.3
H/Total	1	0	0	0	0	0	0	0	1	1	28	7	1	1	0	1	0	5	43	41.8
10:00 10:15									0 0	0 0	6 5	1							6 6	6 6
10:13	1								1	1	6	1 3		1					10	11.3
10:45									0	0	8	1					1		10	9.4
H/Total	1	0	0	0	0	0	0	0	1	1	25	5	0	1	0	0	1	0	32	32.7
11:00 11:15									0 0	0	8 6	2 2							10 8	10 8
11:30									0	0	11	-							11	11
11:45									0	0	7	3	2	1					13	15.3
H/Total 12:00	0	0	0	0	0	0	0	0	0	0	32 12	7	2	1	0	0	0	0	42 14	44.3 14.5
12:15									0	0	7	1	1						8	8
12:30									0	0	10	3		1					14	15.3
12:45	0	0	0	0	0	0	0	0	0	0	15 44	7	1	1	0	0	0	0	17 53	17 54.8
H/Total 13:00	U	0	U	U	U	0	U	0	0	0	7	7	1	1	U	0	0	0	15	15.5
13:15									0	0	10	1	1						12	12.5
13:30									0	0	9	3		1					13	14.3
13:45 H/Total	0	0	0	0	0	0	0	0	0	0	5 31	1 12	2	2	0	0	0	0	7 47	8.3 50.6
14:00				-			-		0	0	11		1	_					12	12.5
14:15									0	0	5	3							8	8
14:30 14:45									0	0	9 7	2 1	1				1		12 9	12.5 8.4
H/Total	0	0	0	0	0	0	0	0	0	0	32	6	2	0	0	0	1	0	41	41.4
15:00									0	0	5	1							6	6
15:15 15:30									0 0	0	8 9		2 1						10 10	11 10.5
15:45									0	0	8	1	1	1		1			12	14.8
H/Total	0	0	0	0	0	0	0	0	0	0	30	2	4	1	0	1	0	0	38	42.3
16:00									0	0	5	1		1					7	8.3
16:15 16:30									0 0	0	3 9	1						1	3 11	3 10.2
16:45									0	0	9								9	9
H/Total	0	0	0	0	0	0	0	0	0	0	26	2	0	1	0	0	0	1	30	30.5
17:00 17:15									0 0	0	13 8	1							13 9	13 9
17:13									0	0	12	3						1	16	15.2
17:45									0	0	17		1						18	18.5
H/Total	0	0	0	0	0	0	0	0	0	0	50	4	1	0	0	0	0	1	56	55.7
18:00 18:15									0 0	0	14 9	2 1	1	1				1	18 11	18.5 11.5
18:30									0	0	14	2	_						16	16
18:45					•		^		0	0	8				•				8	8
H/Total Total	2	0	0	0	0	0	0	0	0 2	2	45 442	5 71	1 17	1 12	0	0 2	0 2	8	53 554	54 572.5
iviai			J	J	J	J	J	, J			774	, , ,		14	J				JJ7	312.3

Project Name: 07700 Hinckley NRFI
Survey Type: Manual Classified Turning Count

Site No: 18



	A - C								A - D											
Time	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)
07:00	13	5							18	18	18	6	1			2			27	29.5
07:15	13		1						14	14.5	32	3	3	2					40	44.1
07:30 07:45	24 27	2			1	1		1	27 36	28 36.2	30 44	6 6	1 1	1		1			37 53	37.5 55.8
H/Total	77	14	1	0	1	1	0	1	95	96.7	124	21	6	3	0	3	0	0	157	166.9
08:00	17	1	 	- ŭ			-		18	18	42	7				1		- ŭ	50	51
08:15	16	4				1			21	22	51	5							56	56
08:30	22	4							26	26	61	3	2						66	67
08:45	12	2							14	14	32	3				2			37	39
H/Total	67	11	0	0	0	1	0	0	79	80	186	18	2	0	0	3	0	0	209	213
09:00 09:15	14 11	3	1						18 15	18 15.5	40 23	3 6	$\begin{bmatrix} 1 \\ 1 \end{bmatrix}$						44 30	44.5 30.5
09:30	6	2	*						8	8	24	3	1						27	27
09:45	6	1	1						8	8.5	18	3		2					23	25.6
H/Total	37	10	2	0	0	0	0	0	49	50	105	15	2	2	0	0	0	0	124	127.6
10:00	3	2		1					6	7.3	15	2	1						18	18.5
10:15	6	2						1	9	8.2	28	1		1					30	31.3
10:30	4	3						1	7 9	7	36 14	1	1 1						37 16	37.5
10:45 H/Total	20	8	0	1	0	0	0	2	31	8.2 30.7	14 93	4	3	1	0	0	0	0	16 101	16.5 103.8
11:00	11		 		-		U		11	11	18	5		1					24	25.3
11:15	6	1							7	7	20	4	1	1					26	27.8
11:30	7	1			1				9	10	19	2		1				2	24	23.7
11:45	7	2	1						10	10.5	15	3	1	1					20	21.8
H/Total	31	4	1	0	1	0	0	0	37	38.5	72	14	2	4	0	0	0	2	94	98.6
12:00	7 7	,	1						8	8.5	13	5	,	1		,		1	20	20.5
12:15 12:30	18	1 2					1		9 20	8.4 20	18 19	3 4	1 1	1		1			24 24	26.8 24.5
12:45	29	5						1	35	34.2	26	5	*						31	31
H/Total	61	8	1	0	0	0	1	1	72	71.1	76	17	2	2	0	1	0	1	99	102.8
13:00	9	2							11	11	12	3						1	16	15.2
13:15	7						1		8	7.4	21								21	21
13:30	13	2					2		17	15.8	16	3							19	19
13:45 H/Total	33	5	0	0	0	0	3	0	5 41	5 39.2	18 67	2 8	0	1	0	0	0	1	21 77	22.3 77.5
14:00	8	2	0	U	0	U	3	U	10	10	17	5	1	1	0	0	0	1	24	25.8
14:15	10	2			1				13	14	12	1	-	1					14	15.3
14:30	10	1	1					1	13	12.7	33	3				1			37	38
14:45	11	2							13	13	40	5	1			1			47	48.5
H/Total	39	7	1	0	1	0	0	1	49	49.7	102	14	2	2	0	2	0	0	122	127.6
15:00	12								12	12	29	5	_						34	34
15:15 15:30	8 5	3							11 6	11 6	19 30	7 3	1					1	28 33	27.7 33
15:45	9				1				10	11	16	5	3			1			25	27.5
H/Total	34	4	0	0	1	0	0	0	39	40	94	20	4	0	0	1	0	1	120	122.2
16:00	12	2							14	14	42	9	1		1		2		55	55.3
16:15	7	2				1			10	11	22	6		1				1	30	30.5
16:30	14	2					2	1	19	17	31	4		1				1	37	37.5
16:45	14	7		_		4	2	1	16	15.2	28	2	-		1			2	32	30.4
H/Total 17:00	47 11	3	0	0	0	1	2	2	59 15	57.2 14.2	123 41	21 6	1	2	1	0	2	4	154 48	153.7 47.4
17:00	15	1			1			1	18	18.2	28	6	1			1		2	38	37.9
17:30	18	4						3	25	22.6	30	1	-			1	1	3	36	34
17:45	11		1						12	12.5	28		1					1	30	29.7
H/Total	55	8	1	0	1	0	0	5	70	67.5	127	13	2	0	0	2	2	6	152	149
18:00	19	1							20	20	42	_							42	42
18:15	11		.						11	11	21	3							24	24
18:30 18:45	9 7	3	1					1	13 8	13.5 7.2	31 26	1 2					1	1	32 30	32 28.6
H/Total	46	4	1	0	0	0	0	1	52	51.7	120	6	0	0	0	0	1	1	128	126.6
Total	547	90	8	1	5	3	6	13	673	672.3	1289	171	26	17	1	12	5	16	1537	1569.3
		•	•	-									•	•	•	•			-	

Project Name: 07700 Hinckley NRFI
Survey Type: Manual Classified Turning Count

Site No: 18



i I	B - A											B - B								
Time	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)	CAR	LGV	OGV 1	OGV 2	BUS	СОАСН	MCY	PCY	TOTAL	TOTAL (PCU)
07:00	3	_						1	4	3.2									0	0
07:15 07:30	6 5	2							8 6	8 6									0	0
07:45	6	1							7	7									0	0
H/Total	20	4	0	0	0	0	0	1	25	24.2	0	0	0	0	0	0	0	0	0	0
08:00 08:15	9 6	1 2	1						10 9	10 9.5									0	0
08:30	7								7	7									0	0
08:45	7	2	1	0	0	0	0	0	7	7	0	0	0	0	0	0	0	0	0	0
H/Total 09:00	29 4	3 2	3	0	0	0	0	0	33 10	33.5 12.8	0	0	0	0	0	0	0	0	0	0
09:15	9	2		1					12	13.3									0	0
09:30 09:45	4 11	5 2		1					10 14	11.3 15.3									0	0
H/Total	28	11	3	4	0	0	0	0	46	52.7	0	0	0	0	0	0	0	0	0	0
10:00	4	2		3					9	12.9									0	0
10:15 10:30	6 6	3					1		10 6	9.4 6									0	0
10:30	4	3							7	7									0	0
H/Total	20	8	0	3	0	0	1	0	32	35.3	0	0	0	0	0	0	0	0	0	0
11:00 11:15	8 7	1 4	2						11 11	12 11									0	0
11:30	6								6	6									0	0
11:45	10	3	2				•	-	15	16									0	0
H/Total 12:00	31 9	8	4	0	0	0	0	0	43 14	45 13.4	0	0	0	0	0	0	0	0	0	0
12:15	6	2					-		8	8									0	0
12:30	9	2	1	1					13	14.8									0	0
12:45 H/Total	12 36	9	2	1	0	1	1	0	15 50	16.5 52.7	0	0	0	0	0	0	0	0	0	0
13:00	8	2	_	_		_	_		10	10	1								1	1
13:15 13:30	7 10	5 1	1 1						13 12	13.5 12.5									0	0
13:45	9	1	1						10	10.5									0	0
H/Total	34	8	3	0	0	0	0	0	45	46.5	1	0	0	0	0	0	0	0	1	1
14:00 14:15	7 10	3 2	3 2	2				1	15 15	19.1 15.2									0	0
14:30	10	2				1		1	13	14									0	0
14:45	5	1					1		7	6.4			_	_	_				0	0
H/Total 15:00	32 12	8	5 2	2	0	1	1	1	50 15	54.7 16	0	0	0	0	0	0	0	0	0	0
15:15	9	1							10	10									0	0
15:30	21	2	2						25	26									0	0
15:45 H/Total	7 49	5	4	0	0	0	0	0	8 58	8 60	0	0	0	0	0	0	0	0	0	0
16:00	14	1	1					<u> </u>	16	16.5								<u> </u>	0	0
16:15	8	4							12	12									0	0
16:30 16:45	14 9	2							18 11	18 11									0	0
H/Total	45	11	1	0	0	0	0	0	57	57.5	0	0	0	0	0	0	0	0	0	0
17:00	17	1					1	4	18	18									0	0
17:15 17:30	7 19	2	1			1	1	1	12 20	11.6 20.5									0	0
17:45	18	1							19	19									0	0
H/Total	61	4	1	0	0	1	1	1	69	69.1	0	0	0	0	0	0	0	0	0	0
18:00 18:15	20 12	3							23 13	23 13									0	0
18:30	15	1							16	16									0	0
18:45 H/Total	14 61	6	0	0	0	0	0	0	15 67	15 67	0	0	0	0	0	0	0	0	0	0
Total	446	85	24	10	0	3	4	3	575	598.2	1	0	0	0	0	0	0	0	1	1

Project Name: 07700 Hinckley NRFI
Survey Type: Manual Classified Turning Count

Site No: 18



	B - C								B - D											
Time	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)
07:00	1								1	1	36	10		1	1	3		1	52	56.5
07:15	2								2	2	55	8		1	1		2		67	68.1
07:30 07:45	1								0	0	65 59	14 12	3 2			,			82 74	83.5 76
H/Total	4	0	0	0	0	0	0	0	4	4	215	44	5	2	2	4	2	1	275	284.1
08:00	3	1		0		0	U	-	4	4	55	9	2		1	7	1		68	69.4
08:15	2	1							3	3	51	12	1	2					66	69.1
08:30	4								4	4	43	9	5	1					58	61.8
08:45		1							1	1	40	4	2	4					50	56.2
H/Total	9	3	0	0	0	0	0	0	12	12	189	34	10	7	1	0	1	0	242	256.5
09:00 09:15	4	1		1					5 1	5 2.3	33 26	10 7	3 5	1				1	46 40	47.5 43
09:30	3	1		1					5	6.3	24	4	3	2					33	37.1
09:45	5								5	5	32	7	2	1					42	44.3
H/Total	12	2	0	2	0	0	0	0	16	18.6	115	28	13	4	0	0	0	1	161	171.9
10:00	5	1	1						7	7.5	27	8	2	1		1			39	42.3
10:15	2	1		1					4	5.3	35	8	2	3		1	_		49	54.9
10:30 10:45	1	1							1	1	29 27	12 5		3			1 1		43 36	43.7 39.3
H/Total	8	3	1	1	0	0	0	0	13	14.8	118	33	4	8	0	2	2	0	167	180.2
11:00	5						5		5	5	28	6	2			1			37	39
11:15	1								1	1	25	4	2	2		1	2		36	39.4
11:30	3	1							4	4	37	5	3	1			1		47	49.2
11:45	3	1							4	4	30	5	2	1			1		39	40.7
H/Total	12	2	0	0	0	0	0	0	14	14	120	20	9	4	0	2	4	0	159	168.3
12:00 12:15	4								4 0	4 0	35 33	12 3	2 3	4					49 43	50 49.7
12:30	1	1							2	2	36	3	5	-		1			45	48.5
12:45	2								2	2	29	2	3	3					37	42.4
H/Total	7	1	0	0	0	0	0	0	8	8	133	20	13	7	0	1	0	0	174	190.6
13:00	5	1							6	6	37	7	3						47	48.5
13:15	3	1							4	4	38	10	2	3			2		55	58.7
13:30 13:45	4 3	1						1	5 4	5 3.2	34 31	6 8	3 2	2 2			1		46 43	49.5 46.6
H/Total	15	3	0	0	0	0	0	1	19	18.2	140	31	10	7	0	0	3	0	191	203.3
14:00	1	1					<u> </u>		2	2	28	6	5	2	<u> </u>				41	46.1
14:15	5		1						6	6.5	30	7	5	1		1	2		46	49.6
14:30		1							1	1	54	7	4	2	1	1			69	75.6
14:45	6						•		6	6	46	10	1	1			2		60	60.6
H/Total 15:00	12	2	1	0	0	0	0	0	15	15.5	158	30	15	6	1	2	4	0	216	231.9 65.5
15:15	1 1	1							2	1 2	46 33	10 9	3	2		1	1 1		62 45	45.9
15:30	2	_							2	2	51	10	3	1	3		_		68	73.8
15:45	2								2	2	50	12	1	1					64	65.8
H/Total	6	1	0	0	0	0	0	0	7	7	180	41	8	4	3	1	2	0	239	251
16:00									0	0	68	17	2	4		1	1		93	99.6
16:15 16:30	1	1							1	1	53 92	9 15	5		1		2		68	71.5
16:30	2 2	1							3 2	3 2	82 73	15 16	6 2	1		2	3 1	1	108 95	111.2 96.9
H/Total	5	1	0	0	0	0	0	0	6	6	276	57	15	5	1	4	5	1	364	379.2
17:00	2								2	2	67	8	1	2	1		1	1	81	83.7
17:15	3								3	3	76	11	6				2	1	96	97
17:30	1	1							2	2	80	10	2	3		1	1		97	102.3
17:45	1								1	1	92	5	4		-		2		103	103.8
H/Total	7	1	0	0	0	0	0	0	8	8	315	34	13	5	1	1	6	2	377	386.8
18:00 18:15	1 4								1 4	1 4	78 69	16 6	3	1		1	2	1 1	101 79	101.8 79.1
18:30	3	2							5	5	56	6					1		63	62.4
18:45	11	1							12	12	50	6	1	1			_		58	59.8
H/Total	19	3	0	0	0	0	0	0	22	22	253	34	5	2	0	1	4	2	301	303.1
Total	116	22	2	3	0	0	0	1	144	148.1	2212	406	120	61	9	18	33	7	2866	3006.9

Project Name: 07700 Hinckley NRFI
Survey Type: Manual Classified Turning Count

Site No: 18



	C - A									C - B										
Time	CAR	LGV	OGV 1	OGV 2	BUS	СОАСН	MCY	PCY	TOTAL	TOTAL (PCU)	CAR	LGV	OGV 1	OGV 2	BUS	СОАСН	MCY	PCY	TOTAL	TOTAL (PCU)
07:00	1				1				2	3									0	0
07:15 07:30	4	2						1	7 12	6.2 12	1								0	0
07:30	10 6	2 2			1			1	10	10.2	1 2								2	1 2
H/Total	21	6	0	0	2	0	0	2	31	31.4	3	0	0	0	0	0	0	0	3	3
08:00	9	2							11	11		1							1	1
08:15	10	4							14	14									0	0
08:30 08:45	5 8	1	2						5 11	5 12	2	1							0 3	0 3
H/Total	32	7	2	0	0	0	0	0	41	42	2	2	0	0	0	0	0	0	4	4
09:00	7	1	1						9	9.5		_							0	0
09:15	6	1							7	7	1								1	1
09:30	6	1							7	7									0	0
09:45 H/Total	9 28	5	1	0	1	0	0	1	13 36	13.2 36.7	1	0	0	0	0	0	0	0	0 1	0
10:00	2		<u> </u>				· ·		2	2	1						-		1	1
10:15	4	1							5	5									0	0
10:30	2								2	2		2							2	2
10:45	5	1	1						6 15	6.5	4	1		1					2 5	3.3
H/Total 11:00	13 5	2	1	0	0	0	0	0	15 7	15.5 7	1	3	2	1	0	0	0	0	2	6.3
11:15	4	1	1						6	6.5	1								1	1
11:30	9	2							11	11									0	0
11:45	4	3							7	7	1	2							3	3
H/Total	22	8	1	0	0	0	0	0	31	31.5	2	2	2	0	0	0	0	0	6	7
12:00 12:15	10 2	1						1	12 2	11.2 2	2 2								2 2	2 2
12:30	4				1			1	6	6.2	1								1	1
12:45	8								8	8	1								1	1
H/Total	24	1	0	0	1	0	0	2	28	27.4	6	0	0	0	0	0	0	0	6	6
13:00 13:15	7 5	2							9	9	1	1							1 5	1 5
13:30	3	$\begin{vmatrix} 1 \\ 1 \end{vmatrix}$							6 4	6 4	4 2	1							2	2
13:45	6	2							8	8	2								2	2
H/Total	21	6	0	0	0	0	0	0	27	27	9	1	0	0	0	0	0	0	10	10
14:00	7	1						1	9	8.2	6								6	6
14:15 14:30	7 5	2					1		8	7.4 7	2								2 3	2 3
14:45	4	2	1						7	7.5	1	1							2	2
H/Total	23	5	1	0	0	0	1	1	31	30.1	12	1	0	0	0	0	0	0	13	13
15:00	5	1	2						8	9	2								2	2
15:15	14	2	_						16	16	1	1							2	2
15:30 15:45	20 5	1 2	1		1				23 7	24.5 7	1 3								1 3	3
H/Total	44	6	3	0	1	0	0	0	54	56.5	7	1	0	0	0	0	0	0	8	8
16:00	10	1	1		_		_		11	11	·	_		1			-	1	0	0
16:15	11	1					1		13	12.4									0	0
16:30	6	2	1						9	9.5	1	_							1	1
16:45 H/Total	18 45	8	1	0	0	0	1	0	22 55	22 54.9	1	1	0	0	0	0	0	0	2	2
17:00	13	1	1					\vdash	15	15.5	±		 						0	0
17:15	14	4							18	18		1							1	1
17:30	20	2							22	22	3								3	3
17:45	20	3	-						23	23	3	4							3	3
H/Total 18:00	67 16	10	1	0	0	0	0	0	78 17	78.5 17	6 1	1	0	0	0	0	0	0	7	7
18:15	12	1						2	15	13.4	4								4	4
18:30	5								5	5	1								1	1
18:45	10	1							11	11									0	0
H/Total	43	3	0	0	0	0	0	2	48	46.4	6	0	0	0	0	0	0	0	6	6
Total	383	66	11	0	5	0	2	8	475	477.9	56	12	2	<u> </u>	0	0	0	0	71	73.3

Project Name: 07700 Hinckley NRFI
Survey Type: Manual Classified Turning Count

Site No: 18



100 100		C - C											C - D										
D7-10 D7-1	Time	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL		CAR	LGV	OGV 1	OGV 2	BUS	СОАСН	MCY	PCY	TOTAL	TOTAL (PCU)		
07:45										0											9		
					1					1							1				12		
															1		2		1		24.2 27.3		
DR:00		0	0	0	1	0	0	0	0	1				0		0	 	0	1	•	72.5		
DB-30		1								1				1							20.5		
DB-68										0	0	26	2	2						30	31		
										,											11		
09-15		1	0		0	0	0	0	0	0					0	0	1	0	0		16 78.5		
09:15		1	0	0	U	0	0	U	0	0					0	0	1	U	0		19		
19945																		1			14.4		
Hyrotal O	09:30									0	0	8		2			1			13	15		
10:00										·											17.2		
10:15 10:30 10:45 10:4		0	0	0	0	0	0	0	0				6	2	0	0	1	1	1		65.6		
10:45													2		2						21 14.6		
10.45										_			2	1	~						9.5		
11:00													3	1							13.5		
11:15	H/Total	0	0	0	0	0	0	0	0	0	0	46	5	2	2	0	0	0	0	55	58.6		
11:30														1							16.5		
11.45											•										6		
												_									14 12		
12:10		0	0	0	0	0	0	0	0					1	0	0	0	0	0		48.5		
12:30																					10		
12:45	12:15									0	0	14	1		1					16	17.3		
H/Total 0 0 0 0 0 0 0 0 0													1								11		
13:00		0	0		0	0		0	0						4	0	1	0	0		12		
13:15		U	U	0	U	0	0	U	0					 	1	0	1	U	0		50.3 12.5		
13:45														-							9		
H/Total 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0										0	0										13		
14:00																	1				14		
14:15 14:30 14:45		0	0	0	0	0	0	0	0					1	0	0	1	0	0		48.5		
14:30																					13 19		
14:45										,											25		
15:00										,				2							21		
15:15	H/Total	0	0	0	0	0	0	0	0	0	0	66	9	2	0	0	0	0	0	77	78		
15:30										0	0								1		13.2		
15:45										ľ											15		
H/Total 0														l .	1						19.5 21.8		
16:00		0	0	0	0	0	0	0	0							0	0	0	1		69.5		
16:30 16:45		-		1	_			-						1				-			21.7		
16:45	16:15									0	0	18								21	21		
H/Total 0 0 0 0 0 0 0 94 15 1 0 0 0 1 111 17:00 1 1 1 1 37 7 7 1 1 45 17:15 0 0 0 25 3 1 29 17:30 0 0 30 3 33 33 17:45 0 0 0 32 2 2 H/Total 1 0 0 0 0 1 1 1 2 0 0 1 1 1 36 H/Total 1 0 0 0 0 0 1 1 1 2 0 0 1																					39		
17:00 1 17:15 0 17:30 17:45 17:45 17:45 17:45 18:00 18:15 18:30 18:45 11 11 11 11 12 13 14 15 1 <		0			0			0						1				0	4		29		
17:15 0 0 0 25 3 1 0 29 33 33 33 33 33 33 33 36 33 36 33 36			U	1 0	U	U	U	U	U					1	U	U	U		1		110.7 44.4		
17:30 17:45 H/Total 1 0 0 0 0 30 3 2 2 2 36 H/Total 1 0 0 0 0 0 1 1 124 15 1 2 0 0 1 0 143 18:00 18:15 0 0 0 0 24 1 1 1 1 2 29 18:30 1 1 1 1 1 1 1 15 1 18:45 0 0 0 15 1 0 0 2 18		1												1				1			29.5		
H/Total 1 0 0 0 0 0 0 1 1 124 15 1 2 0 0 1 0 143 18:00 18:15 1 1 1 1 1 1 1 1 2 29 18:30 1 <td></td> <td>_</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>33</td>														_							33		
18:00 18:15 18:30 18:45 0 0 33 1 0 0 24 1 1 1 1 2 15 1 1 1 1 1 <td>\vdash</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0</td> <td>0</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>38.6</td>	\vdash									0	0										38.6		
18:15 18:30 18:45		1	0	0	0	0	0	0	0					1	2	0	0	1	0		145.5		
18:30 1 18:45 1 1 1																					34		
18:45 0 0 15 1 2 18		1								1	1					1	1		2		29.4 15		
		1								0	0		_						2		16.4		
		1	0	0	0	0	0	0	0					0	0	1	1	0			94.8		
Total 3 0 0 1 0 0 0 0 4 5.3 765 94 17 7 1 8 2 8 902		3	0	0	1	0	0	0	0	4	5.3	765	94	17	7	1	8	2	8	902	921		

Project Name: 07700 Hinckley NRFI
Survey Type: Manual Classified Turning Count

Site No: 18



	D - A											D - B										
Time	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)	CAR	LGV	OGV 1	OGV 2	BUS	СОАСН	MCY	PCY	TOTAL	TOTAL (PCU)		
07:00	9	3	1					1	14	13.7	48	6	4	2	1	2	1		64	71		
07:15	16	4	1	1	_				22	23.8	65	17	5	1	1	1	1	_	91	96.2		
07:30 07:45	22 25	4 5			1	1	1	3	32 30	31 30	76 75	11 19	4	3			1	1 1	93 102	93.6 107.1		
H/Total	72	16	2	1	1	1	1	4	98	98.5	264	53	17	6	2	3	3	2	350	367.9		
08:00	27	5		_		_	1	T	33	32.4	90	13	1 1/	1			1	1	106	105.9		
08:15	33	2						1	36	35.2	59	9	6				2	1	77	78		
08:30	31	3							34	34	53	8	4	1					66	69.3		
08:45	44	6				1	1		52	52.4	69	12	4	2		1			88	93.6		
H/Total	135	16	0	0	0	1	2	1	155	154	271	42	14	4	0	1	3	2	337	346.8		
09:00 09:15	23 16	3 7	1	1 1			1		28 24	27.9 25.3	52 38	9 6	2	2 2	3	1	2 1	2	73 51	80.4 52.4		
09:13	22	3	1	1					27	28.8	34	5	6	6			1	۷	51	61.8		
09:45	16	1	_	3					20	23.9	31	12	2	3		1		1	50	55.1		
H/Total	77	14	2	5	0	0	1	0	99	105.9	155	32	14	13	3	2	3	3	225	249.7		
10:00	21	3		2					26	28.6	28	9	3	1		1	1		43	46.2		
10:15	18	3	2						23	24	32	4	2	1			1		40	41.7		
10:30	18	5	.						23	23	26	8	4	1	4				39	42.3		
10:45 H/Total	20 77	4 15	3	2	0	0	0	3	28 100	26.1 101.7	36 122	9 30	10	2 5	1	1	2	0	49 171	53.1 183.3		
11:00	23	2	3	1	U	U	U	3	26	27.3	32	9	10	1	1	1	1	1	46	47.4		
11:15	18	4		2					24	26.6	36	3	7	_			-	-	46	49.5		
11:30	21	7	1					1	30	29.7	32	10	2						44	45		
11:45	27	3	2	1					33	35.3	33	3				1			37	38		
H/Total	89	16	3	4	0	0	0	1	113	118.9	133	25	10	1	0	2	1	1	173	179.9		
12:00	26	5	1				1		33	32.9	42	4		1		1	2	1	51	51.3		
12:15 12:30	18 18	6	1 1	1					26 24	27.8 25.8	29 23	1 2	1 3	2			2		35 30	36.9 34.1		
12:30	21	4 6	1 1	1					28	29.3	23 27	2	6						35	38		
H/Total	83	21	3	3	0	0	1	0	111	115.8	121	9	10	5	0	1	4	1	151	160.3		
13:00	23	1		1	-			-	25	26.3	34	5		-	-				39	39		
13:15	18	5							23	23	35	6	1	3					45	49.4		
13:30	24	7							31	31	31	12	1						44	44.5		
13:45	21	3	2						26	27	20	4	2	2		2	- 0		28	31		
H/Total 14:00	86 15	16 3	2	1	0	0	0	0	105 21	107.3 23	120 33	27 4	1	3	0	2	0	0	156 41	163.9 43.2		
14:15	18	3	2						23	23 24	35	4	1 1	2		1	1		42	45.1		
14:30	19	2							21	21	32	14	2	2					50	53.6		
14:45	21	3	2					1	27	27.2	42	4	2	2					50	53.6		
H/Total	73	11	6	0	0	1	0	1	92	95.2	142	26	6	7	0	1	1	0	183	195.5		
15:00	43	4	2						49	50	47	11	1	1					60	61.8		
15:15	30	4	1			2	1		38	39.9	42	12	2		_		_		56	57		
15:30 15:45	36 38	3	2	1		2			42 48	44.3 50.5	47 38	7 15	2	1	2	1	1		61 56	65.7 58.8		
H/Total	38 147	18	6	1	0	2 4	1	0	48 177	184.7	174	45	6	3	2	2	1	0	233	243.3		
16:00	35	3		1		T			39	40.3	50	13	2	1		1	±		67	70.3		
16:15	38	6	2						46	47	46	9	1	2	1	_	1		60	63.5		
16:30	32	2							34	34	62	10	1			1			74	75.5		
16:45	43	5	1						49	49.5	80	10	1	2		2	1	1	97	100.7		
H/Total	148	16	3	1	0	0	0	0	168	170.8	238	42	5	5	1	4	2	1	298	310		
17:00	46 57	5	1			1 1			53 63	54.5 64	67 62	17 5	3	3			3	1	90 73	95.4		
17:15 17:30	62	5 4	1	1		1 1		1	63 70	72	62 49	5 4	1	1 1			3	1 2	73 56	72.2 55.7		
17:45	33	3	1				1	2	39	36.8	58	8		•			1	_	67	66.4		
H/Total	198	17	2	1	0	3	1	3	225	227.3	236	34	4	5	0	0	4	3	286	289.7		
18:00	42	10				1			53	54	41	4		2		1		2	50	52		
18:15	44	3						1	48	47.2	52	2		1			1	2	58	57.1		
18:30	35	3	1	1 1					40	41.8	42	5	1	1		1		1	51	53		
18:45	28	16	1	1	0	1	0	1	29 170	28.2	38	1.4	1	1 5	0	7	1	F	42	43.3		
H/Total Total	149 1334	16 192	33	1 20	0	11	0 7	2 15	170 1613	171.2 1651.3	173 2149	14 379	101	5 62	9	2 21	1 25	5 18	201 2764	205.4 2895.7		
Total	1004	172	ا ا	_ ∠∪	1	11	/	1 12	1012	1031.3	Z143	3/3	101	02	9	_ <u> </u>	23	10	2/04	2033./		

Project Name: 07700 Hinckley NRFI
Survey Type: Manual Classified Turning Count

Site No: 18



	D - C												D - D									
Time	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)		
07:00	16	1	_						17	17									0	0		
07:15 07:30	23 16	7 5	1	2					31 23	31.5 25.6									0	0		
07:45	20	4				1			25	26									0	0		
H/Total	75	17	1	2	0	1	0	0	96	100.1	0	0	0	0	0	0	0	0	0	0		
08:00 08:15	32 18	1 2							33 20	33 20									0	0		
08:30	29	1							30	30									0	0		
08:45	30	3 7	0	1	1	0	0	0	35	37.3	0	0	0	0	0	0	0	0	0	0		
H/Total 09:00	109 20	2	0	1	1	0	0	0	118 24	120.3 25.8	0	0	0	0	0	0	0	0	0	0		
09:15	14	3				1	1		19	19.4									0	0		
09:30 09:45	11 16	4	1 1			1			16 19	16.5 20.5	1								0	0 1		
H/Total	61	10	3	1	0	2	1	0	78	82.2	1	0	0	0	0	0	0	0	1	1		
10:00	10	3				1	1		15	15.4									0	0		
10:15 10:30	10 12	2	2	1 1				1	14 15	14.5 17.3									0	0		
10:30	10	4							14	17.3									0	0		
H/Total	42	9	2	2	0	1	1	1	58	61.2	0	0	0	0	0	0	0	0	0	0		
11:00 11:15	11 17	1 2							12 19	12 19									0	0		
11:30	15								15	15									0	0		
11:45	12							1	13	12.2									0	0		
H/Total 12:00	55 15	3	0	0	0	0	0	1	59 15	58.2 15	0	0	0	0	0	0	0	0	0	0		
12:15	8	1						1	10	9.2									0	0		
12:30	14	3						1	18	17.2									0	0		
12:45 H/Total	11 48	6	0	0	0	0	0	2	13 56	13 54.4	0	0	0	0	0	0	0	0	0	0		
13:00	11	<u> </u>	<u> </u>	Ŭ		Ŭ	<u> </u>		11	11		<u> </u>		Ů	<u> </u>	Ŭ	<u> </u>	<u> </u>	0	0		
13:15	12	2	1	1					16	17.8									0	0		
13:30 13:45	9 14	2	2						13 16	14 16.5									0	0		
H/Total	46	5	4	1	0	0	0	0	56	59.3	0	0	0	0	0	0	0	0	0	0		
14:00	7	2		1					10	11.3									0	0		
14:15 14:30	10 22	3 4	1						13 27	13 27.5									0	0		
14:45	17	1							18	18	1								1	1		
H/Total	56 17	10	1	1	0	0	0	0	68	69.8	1	0	0	0	0	0	0	0	1	1		
15:00 15:15	17 20	4 7				1			21 28	21 29									0	0		
15:30	16	4							20	20	1								1	1		
15:45	18 71	10		0	0	1	0	0	23	24	1	0	0	0	0	0	0		0	0		
H/Total 16:00	14	19 2	0	0	0	2	0	0	92 16	94 16	1	0	0	0	0	0	0	0	0	0		
16:15	19					1			20	21									0	0		
16:30	18	1			1	,	1		21	21.4 20									0	0		
16:45 H/Total	14 65	7	0	0	1	2	1	0	19 76	78.4	0	0	0	0	0	0	0	0	0	0		
17:00	35	3		1		1		-	40	42.3	-						-		0	0		
17:15 17:30	23 19	3				1			27 22	28 22									0 0	0		
17:30 17:45	23	3	1						27	22 27.5									0	0		
H/Total	100	12	1	1	0	2	0	0	116	119.8	0	0	0	0	0	0	0	0	0	0		
18:00	19 16	2					2		23	21.8									0	0		
18:15 18:30	16 22	3 1						6	19 29	19 24.2									0	0		
18:45	14								14	14									0	0		
H/Total	71	6	0	0	0	0	2	6	85 059	79 076 7	0	0	0	0	0	0	0	0	0	0		
Total	799	111	12	9	2	10	5	10	958	976.7	3	0	0	0	0	0	0	0	3	3		

Project Name: 07700 Hinckley NRFI
Survey Type: Manual Classified Turning Count

Site No: 18



	From A										То А									
Time	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)
07:00	44	13	1	2	0	2	0	0	62	67.1	13	3	1	0	1	0	0	2	20	19.9
07:15 07:30	53 65	4	5	2	0	0	0	0	64 78	69.1 79.5	26 37	8 7	1 0	1 0	0	0	0	1 3	37 50	38 49
07:30	84	11 16	1 1	0	1	1 1	0	0	105	108	37 37	8	0	0	1 1	0	1 0	1	47	47.2
H/Total	246	44	8	5	1	4	0	1	309	323.7	113	26	2	1	3	1	1	7	154	154.1
08:00	73	8	0	0	0	1	0	0	82	83	45	8	0	0	0	0	1	0	54	53.4
08:15	87	11	0	0	0	1	0	0	99	100	49	8	1	0	0	0	0	1	59	58.7
08:30	93	8	3	1	0	0	0	0	105	107.8	43	3	0	0	0	0	0	0	46	46
08:45	54	7	1	0	0	2	0	0	64	66.5	59	7	2	0	0	1	1	0	70	71.4
H/Total 09:00	307 62	34 13	1	0	0	4 0	0	0	350 76	357.3 76.5	196 34	26 6	3 5	1	0	0	2	0	229 47	229.5 50.2
09:15	48	9	2	0	0	0	0	0	59	60	32	10	0	2	0	0	0	0	44	46.6
09:30	35	5	1	0	0	0	0	0	41	41.5	32	9	1	2	0	0	0	0	44	47.1
09:45	26	5	1	3	0	1	0	5	41	42.4	36	5	0	4	1	0	0	1	47	52.4
H/Total	171	32	5	3	0	1	0	5	217	220.4	134	30	6	9	1	0	1	1	182	196.3
10:00	24	4	1	1	0	0	0	0	30	31.8	27	5	0	5	0	0	0	0	37	43.5
10:15 10:30	39 47	4 6	0	1 1	0	0	0	1 0	45 55	45.5 56.8	28 27	7 5	0	0	0	0	1 0	0	38 32	38.4 32
10:30	47 29	3	1 1	0	0	0	1	1	35	34.1	27 29	7	2	0	0	0	0	3	41	39.6
H/Total	139	17	3	3	0	0	1	2	165	168.2	111	24	4	5	0	0	1	3	148	153.5
11:00	37	7	0	1	0	0	0	0	45	46.3	36	5	2	1	0	0	0	0	44	46.3
11:15	32	7	1	1	0	0	0	0	41	42.8	29	9	1	2	0	0	0	0	41	44.1
11:30	37	3	0	1	1	0	0	2	44	44.7	36	9	1	0	0	0	0	1	47	46.7
11:45	29	8	4	2	0	0	0	0	43	47.6	41	9	4	1	0	0	0	0	55	58.3
H/Total 12:00	135 32	25 6	5 2	5 1	0	0	0	2 1	173 42	181.4 43.5	142 45	32 10	8	0	0	0	2	1	187 59	195.4 57.5
12:15	32	5	1	1 1		1	1	0	41	43.2	26	8	1	1	0	0	0	0	36	37.8
12:30	47	9	1	1	0	0	0	0	58	59.8	31	6	2	2	1	0	0	1	43	46.8
12:45	70	12	0	0	0	0	0	1	83	82.2	41	7	1	1	0	1	0	0	51	53.8
H/Total	181	32	4	3	0	1	1	2	224	228.7	143	31	5	4	1	1	2	2	189	195.9
13:00	28	12	1	0	0	0	0	1	42	41.7	38	5	0	1	0	0	0	0	44	45.3
13:15 13:30	38 38	1 8	0	0	0	0	1 2	0 0	41 49	40.9 49.1	30 37	11 9	1 1	0	0	0	0 0	0	42 47	42.5 47.5
13:45	27	4	0	2	0	0	0	0	33	35.6	36	5	3	0	0	0	0	0	44	45.5
H/Total	131	25	2	3	0	0	3	1	165	167.3	141	30	5	1	0	0	0	0	177	180.8
14:00	36	7	2	1	0	0	0	0	46	48.3	29	7	5	2	0	1	0	1	45	50.3
14:15	27	6	0	1	1	0	0	0	35	37.3	35	5	4	0	0	0	1	1	46	46.6
14:30	52	6	2	0	0	1	0	1	62	63.2	34	6	0	0	0	1	0	0	41	42
14:45 H/Total	58 173	8 27	5	2	0	2	1	0 1	69 212	69.9 218.7	30 128	6 24	3 12	2	0	2	2	3	41 173	41.1 180
15:00	46	6	0	0	0	0	0	0	52	52	60	6	6	0	0	0	0	0	72	75
15:15	35	10	3	0	o o	0	0	1	49	49.7	53	7	1	0	0	2	1	0	64	65.9
15:30	44	4	1	0	0	0	0	0	49	49.5	77	6	5	1	1	0	0	0	90	94.8
15:45	33	6	4	1	1	2	0	0	47	53.3	50	10	1	0	0	2	0	0	63	65.5
H/Total	158	26	8	1	1	2	0	1	197	204.5	240	29	13	1	1	4	1	0	289	301.2
16:00	59	12 8	1 1	1		0	2	0	76	77.6 44.5	59 57	5 11	1 2	1 0	0	0	0	0	66 71	67.8
16:15 16:30	32 54	8 7	0	1 1	0	0	0 2	3	43 67	44.5 64.7	57 52	11 8	2	0	0	0	0	0	71 61	71.4 61.5
16:45	51	3	0	0	0	0	0	3	57	54.6	70	11	1	0	0	0	0	0	82	82.5
H/Total	196	30	1	3	1	1	4	7	243	241.4	238	35	5	1	0	0	1	0	280	283.2
17:00	65	9	0	0	0	0	1	1	76	74.6	76	7	2	0	0	1	0	0	86	88
17:15	51	8	1	0	1	1	0	3	65	65.1	78	11	0	0	0	2	1	1	93	93.6
17:30	60	8	0	0	0	1	1	7	77	71.8	101	6	2	1	0	1	0	1	112	114.5
17:45 H/Total	56 232	0 25	3	0	0	2	0	1 12	60 278	60.7 272.2	71 326	7 31	4	1	0	4	1 2	2 4	81 372	78.8 374.9
18:00	75	3	0	1	0	0	0	12	80	80.5	78	14	0	0	0	1	2 0	0	93	94
18:15	41	4	1	0	0		0	0	46	46.5	68	5	0	0	0	0	0	3	76	73.6
18:30	54	6	1	0	0	0	0	0	61	61.5	55	4	1	1	0	0	0	0	61	62.8
18:45	41	2	0	0	0	0	1	2	46	43.8	52	2	0	0	0	0	0	1	55	54.2
H/Total	211	15	2	1	0	0	1	3	233	232.3	253	25	1	1	0	1	0	4	285	284.6
Total	2280	332	51	30	6	17	13	37	2766	2816.1	2165	343	68	30	6	14	13	26	2665	2729.4

Project Name: 07700 Hinckley NRFI
Survey Type: Manual Classified Turning Count

Site No: 18



	From B										То В									
Time	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)
07:00	40	10	0	1	1	3	0	2	57 77	60.7	61	8	4	4	1	2	1	0	81	90.6
07:15 07:30	63 71	10 15	0 3	0	0	0 0	2 0	0 0	77 89	78.1 90.5	73 88	18 14	6 4	0	1 0	0	1 1	0 1	101 108	106.7 108.6
07:45	65	13	2	0	0	1	0	0	81	83	90	22	4	3	0	0	0	1	120	125.1
H/Total	239	48	5	2	2	4	2	2	304	312.3	312	62	18	8	2	3	3	2	410	431
08:00 08:15	67 59	11 15	2 2	0 2	0	0 0	1 0	0 0	82 78	83.4 81.6	104 79	14 11	0 6	0	0 0	0	1 2	1 1	121 99	120.9 100
08:30	54	9	5	1	0	0	0	0	69	72.8	63	9	5	2	0	0	0	0	79	84.1
08:45	47 227	5 40	2	4 7	0	0	0	0	58	64.2 302	81	15	5	2 5	0	1	0	0	104	110.1
H/Total 09:00	41	13	11 6	1	0	0	0	0	287 61	65.3	327 60	49 15	16 4	2	3	1	3 2	2 0	403 87	415.1 94.4
09:15	35	9	5	3	0	0	0	1	53	58.6	52	6	2	2	0	0	1	2	65	66.4
09:30	31	10 9	3	4 2	0	0	0	0	48	54.7	39 33	5	7	6 4	0	0	0	0	57 60	68.3
09:45 H/Total	48 155	41	2 16	10	0	0	0	0	61 223	64.6 243.2	184	13 39	2 15	14	3	3	3	6 8	269	63.4
10:00	36	11	3	4	0	1	0	0	55	62.7	35	9	3	1	0	1	1	0	50	53.2
10:15 10:30	43 36	12 12	2	4	0 0	1 0	1	0 0	63 50	69.6 50.7	37 32	5 13	2	1 2	0	0	1	0	46 51	47.7 55.6
10:30	36 31	12 9	0	3	0	0	1	0	50 44	50.7 47.3	32 44	13 11	4	3	0 1	0	0 1	0	61	65.8
H/Total	146	44	5	12	0	2	3	0	212	230.3	148	38	10	7	1	1	3	0	208	222.3
11:00	41	7	4	0	0	1	0	0	53	56	40	11	3	1	0	1	1	1	58	60.4
11:15 11:30	33 46	8 6	2 3	2 1	0 0	0	2 1	0 0	48 57	51.4 59.2	43 43	5 10	2	0	0 0	0	0 0	0	55 55	58.5 56
11:45	43	9	4	1	0	0	1	0	58	60.7	41	8	2	1	0	1	0	0	53	56.3
H/Total	163	30	13	4	0	2	4	0	216	227.3	167	34	14	2	0	2	1	1	221	231.2
12:00 12:15	48 39	16 5	2 3	0 4	0	0 0	0	0 0	67 51	67.4 57.7	56 38	5 2	1 1	2	0 0	0	2 2	0	67 45	67.8 46.9
12:30	46	6	6	1	0	1	0	0	60	65.3	34	5	3	3	0	0	0	0	45	50.4
12:45	43	3	4	3	0	1	0	0	54	60.9	43	4	6	0	0	0	0	0	53	56
H/Total 13:00	176 51	30 10	15 3	8	0	0	0	0	232 64	251.3 65.5	171 43	16 12	11	6 0	0	0	0	0	210 56	221.1 56.5
13:15	48	16	3	3	0	0	2	0	72	76.2	49	8	2	3	0	0	0	0	62	66.9
13:30	48	8	4	2	0	0	1	0	63	67	42	15	1	1	0	0	0	0	59	60.8
13:45 H/Total	43 190	8 42	13	7	0	0	3	1	57 256	60.3 269	27 161	5 40	6	5	0	2	0	0	37 214	41.3 225.5
14:00	36	10	8	4	0	0	0	0	58	67.2	50	4	2	1	0	1	1	0	59	61.7
14:15	45	9	8	1	0	1	2	1	67	71.3	42	7	1	2	0	0	0	0	52	55.1
14:30 14:45	64 57	10 11	4	2	0	2 0	0 3	0	83 73	90.6 73	44 50	16 6	3 2	2	0	0	0	0	65 61	69.1 64
H/Total	202	40	21	8	1	3	5	1	281	302.1	186	33	8	7	0	1	2	0	237	249.9
15:00	59	11	5	2	0	0	1	0	78	82.5	54	12	1	1	0	0	0	0	68	69.8
15:15 15:30	43 74	11 12	1 5	1	0	1 1	1 0	0	57 95	57.9 101.8	51 57	13 7	4 3	0	0 2	0	0 1	0	68 72	70 77.2
15:45	59	13	1	1	0	0	0	0	74	75.8	49	16	2	2	0	2	0	0	71	76.6
H/Total	235	47	12	4	3	1	2	0	304	318	211	48	10	4	2	3	1	0	279	293.6
16:00 16:15	82 62	18 13	3 5	4 0	0 1	1 0	1 0	0 0	109 81	116.1 84.5	55 49	14 9	2	2	0 1	0	0 1	0	74 63	78.6 66.5
16:30	98	20	6	0	0	2	3	0	129	132.2	72	11	1	0	0	1	0	1	86	86.7
16:45	84	18	2	1	0	1	1	1	108	109.9	89	11	1	2	0	2	1	1	107	110.7
H/Total 17:00	326 86	69 9	16 1	5 2	1	4 0	5	1	427 101	442.7 103.7	265 80	45 17	5 3	6 3	0	4 0	2 0	2 0	330 103	342.5 108.4
17:00	86	13	6	0	0	1 1	3	2	111	111.6	70	7	1	1	0	0	3	1	83	82.2
17:30	100	11	3	3	0	1 1	1	0	119	124.8	64	7	0	1	0	0	0	3	75	73.9
17:45 H/Total	111 383	6 39	4 14	0 5	0	2	7	3	123 454	123.8 463.9	78 292	8 39	1 5	0 5	0	0	4	0 4	88 349	87.9 352.4
18:00	99	19	3	1	0	0	2	1	125	125.8	56	6	0	3	0	1	0	3	69	71.5
18:15	85	7	1	0	0	1 1	1	1	96	96.1	65	3	1	1	0	0	1	2	73	72.6
18:30	74	9	0	0	0	0	1	0	84	83.4	57 46	7	1	1	0	1	0	1	68 50	70 51.2
18:45 H/Total	75 333	8 43	5	2	0	0	0 4	0 2	85 390	86.8 392.1	46 224	3 19	2	6	0	2	0 1	0 6	50 260	51.3 265.4
Total	2775	513	146	74	9	21	37	11	3586	3754.2	2648	462	120	75	9	23	27	26	3390	3542.5

Project Name: 07700 Hinckley NRFI
Survey Type: Manual Classified Turning Count

Site No: 18



	From C									То С										
Time	CAR	LGV	OGV 1	OGV 2	BUS	СОАСН	MCY	PCY	TOTAL	TOTAL (PCU)	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)
07:00	9	1	0	0	1	0	0	0	11	12	30	6	0	0	0	0	0	0	36	36
07:15 07:30	11 33	5 4	0	1 0	0	1 0	0	1	19 38	20.5 37.2	38	7 7	2 0	2	0 0	0	0 0	0	48 51	50.3 54.6
07.30	26	5	0	1	1	2	0	1	36	39.5	41 47	11		0	1	1 1	0	1	61	62.2
H/Total	79	15	0	2	2	3	0	3	104	109.2	156	31	2	3	1	2	0	1	196	203.1
08:00	26	4	1	0	0	1	0	0	32	33.5	53	3	0	0	0	0	0	0	56	56
08:15	36	6	2	0	0	0	0	0	44	45	36	7	0	0	0	1	0	0	44	45
08:30	16	0	0	0	0	0	0	0	16	16	55	5	0	0	0	0	0	0	60	60
08:45 H/Total	22 100	3 13	7	0	0	0	0	0	29 121	31 125.5	42 186	6 21	0	1	1	0	0	0	50 210	52.3 213.3
09:00	25	2	1	0	0	0	0	0	28	28.5	38	7	1	1	0	0	0	0	47	48.8
09:15	19	3	0	0	0	0	1	0	23	22.4	25	6	1	1	0	1	1	0	35	37.2
09:30	14	3	2	0	0	1	0	0	20	22	20	7	1	1	0	0	0	0	29	30.8
09:45	25	3	0	0	1	0	0	2	31	30.4	27	2	2	0	0	1	0	0	32	34
H/Total	83	11	3	0	1	1	1	2	102	103.3	110	22	5	3	0	2	1	0	143	150.8
10:00 10:15	24 12	0 3	0	0 2	0 0	0	0	0	24 17	24 19.6	18 18	6 5	0	1 2	0 0	0	1 0	0 2	28 27	30.2 28
10:13	10	2	1	0	0		0	0	13	13.5	17	3	2	1	0	0	0	0	23	25.3
10:45	14	4	2	1	0	0	0	0	21	23.3	17	6	0	0	0	0	0	1	24	23.2
H/Total	60	9	3	3	0	0	0	0	75	80.4	70	20	3	4	0	1	1	3	102	106.7
11:00	19	3	3	0	0	0	0	0	25	26.5	27	1	0	0	0	0	0	0	28	28
11:15 11:30	10 18	2	1 0	0	0	0	0	0	13 25	13.5 25	24 25	3 2	0	0	0 1	0	0 0	0	27 28	27 29
11:30	16 16	6	0	0	0	0	0	0	25 22	25 22	25 22	3	1	0	0	0	0	1	28 27	26.7
H/Total	63	18	4	0	0	0	0	0	85	87	98	9	1	0	1	0	0	1	110	110.7
12:00	22	1	0	0	0	0	0	1	24	23.2	26	0	1	0	0	0	0	0	27	27.5
12:15	18	1	0	1	0	0	0	0	20	21.3	15	2	0	0	0	0	1	1	19	17.6
12:30	15	1	0	0	1	0	0	1	18	18.2	33	6	0	0	0	0	0	1	40	39.2
12:45	17	2	0	0	0	1	0	0	20	21	42	7	0	0	0	0	0	1	50	49.2
H/Total 13:00	72 17	5 4	0	0	0	0	0	0	82 22	83.7 22.5	116 25	15 3	0	0	0	0	0	3 0	136 28	133.5 28
13:15	17	3	0			0	0	0	20	20	22	3	1	1	0	0	1	0	28	29.2
13:30	15	4	0	0	0	0	0	0	19	19	26	5	2	0	0	0	2	0	35	34.8
13:45	20	2	0	0	0	1	0	0	23	24	21	2	1	0	0	0	0	1	25	24.7
H/Total	69	13	1	0	0	1	0	0	84	85.5	94	13	4	1	0	0	3	1	116	116.7
14:00 14:15	24 26	3 2	0	0	0	0	0	1	28	27.2	16	5	0	1	0	0	0	0	22	23.3
14:15	26 31	4	0			0	0	0	29 35	28.4 35	25 32	5 6	2	0	0	0	0 0	0	32 41	33.5 41.2
14:45	20	6	3	0	0	0	0	0	29	30.5	34	3	0	0	0	0	0	0	37	37
H/Total	101	15	3	0	0	0	1	1	121	121.1	107	19	3	1	1	0	0	1	132	135
15:00	19	2	2	0	0	0	0	1	24	24.2	30	4	0	0	0	0	0	0	34	34
15:15	26	7	0	0	0	0	0	0	33	33	29	11	0	0	0	1	0	0	41	42
15:30 15:45	36 25	4	2	0	1 0	0	0	0	43 30	45 31.8	23 29	5 4	0	0	0	0	0 0	0	28 35	28 37
H/Total	106	16	5	1	1	0	0	1	130	134	111	24	0	0	1	2	0	0	138	141
16:00	25	6	1	0	0	0	0	1	33	32.7	26	4	0	0	0	0	0	0	30	30
16:15	29	4	0	0	0	0	1	0	34	33.4	27	2	0	0	0	2	0	0	31	33
16:30	42	6	1	0	0	0	0	0	49	49.5	34	4	0	0	1	0	3	1	43	41.4
16:45	44	8	0	0	0	0	0	0	52	52	30	5	0	0	0	1	0	1	37	37.2
H/Total 17:00	140 51	24 8	2	0	0	0	1	0	168 61	167.6 60.9	117 49	15 6	0	0	0	3	3 0	2	141 58	141.6 59.5
17:00	39	8	1 1	0	0	0	0	0	48	48.5	49	4	0	0	1	1	0	1	48	49.2
17:30	53	5	0	0	0	0	0	0	58	58	38	8	0	0	0	0	0	3	49	46.6
17:45	55	5	0	2	0	0	0	0	62	64.6	35	3	2	0	0	0	0	0	40	41
H/Total	198	26	2	2	0	0	1	0	229	232	163	21	2	1	1	2	0	5	195	196.3
18:00	50	2	0	0	0	0	0	0	52	52	39	3	0	0	0	0	2	0	44	42.8
18:15 18:30	40 21	2		0	1 0	1 0	0	4 0	48 22	46.8 22	31 35	3 6	0	0	0	0	0	0 6	34 48	34 43.7
18:30	21 25	2	0	0	0	0	0	2	22 29	22 27.4	35	1	0	0	0	0	0	1	48 34	33.2
H/Total	136	7	0	0	1	1	0	6	151	148.2	137	13	1	0	0	0	2	7	160	153.7
Total	1207	172	30	9	6	8	4	16	1452	1477.5	1465	223	22	14	7	13	11	24	1779	1802.4

Project Name: 07700 Hinckley NRFI
Survey Type: Manual Classified Turning Count

Site No: 18



	From D									To D										
Time	CAR	LGV	OGV 1	OGV 2	BUS	СОАСН	MCY	PCY	TOTAL	TOTAL (PCU)	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)
07:00	73	10	5	2	1	2	1	1	95	101.7	62	17	1	1	1	5	0	1	88	95
07:15 07:30	104 114	28 20	7 4	2 2	1 1	1 1	1 2	0	144 148	151.5 150.2	94 117	14 22	3 4	3	0	0	2 0	0	118 144	124.2 145.2
07:30	120	28	4	3	0	1	0	4	157	163.1	121	22	3	2	0	4	0	0	151	159.1
H/Total	411	86	20	9	3	5	4	6	544	566.5	394	74	11	6	2	10	2	2	501	523.5
08:00	149	19	0	1	0	0	2	1	172	171.3	113	17	3	0	1	2	1	0	137	140.9
08:15	110	13	6	0	0	0	2	2	133	133.2	128	19	3	2	0	0	0	0	152	156.1
08:30	113	12	4	1	0	0	0	0	130	133.3	115	12	7	1	0	0	0	0	135	139.8
08:45 H/Total	143 515	21 65	14	3 5	1	2	5	3	175 610	183.3 621.1	84 440	8 56	17	7	1	2	0	0	102 526	111.2 548
09:00	95	14	6	3	3	1	3	0	125	134.1	91	14	4	0	0	0	0	0	109	111
09:15	68	16	2	3	0	1	2	2	94	97.1	61	15	6	1	0	0	1	1	85	87.9
09:30	67	12	8	7	0	0	0	0	94	107.1	56	9	5	2	0	1	0	0	73	79.1
09:45	64	14	3	6	0	2	0	1	90	100.5	67	11	2	3	0	0	0	1	84	88.1
H/Total 10:00	294 59	56 15	19 3	19 3	3	2	5 2	3 0	403 84	438.8 90.2	275 63	49 10	17 3	6 1	0	1	0	0	351 78	366.1 81.8
10:00	60	9	4	2	0	0	1	1	77	90.2 80.2	71	11	2	6	0	1 1	0	0	91	100.8
10:30	56	13	6	2	0	0	0	0	77	82.6	73	12	2	1	0	0	1	0	89	90.7
10:45	66	17	2	2	1	0	0	3	91	93.2	50	9	2	3	0	0	1	0	65	69.3
H/Total	241	54	15	9	1	2	3	4	329	346.2	257	42	9	11	0	2	2	0	323	342.6
11:00	66	12	1 7	2	0	1	1	1	84	86.7	60	12	3	1	0	1	0	0	77	80.8
11:15 11:30	71 68	9 17	3	2	0	0 0	0	0	89 89	95.1 89.7	50 65	9 12	3	3 2	0	0	2 1	0 2	68 85	73.2 86.9
11:45	72	6	2	1	0	1	0	1	83	85.5	56	9	3	2	0	0	1	0	71	74.5
H/Total	277	44	13	5	0	2	1	3	345	357	231	42	12	8	0	2	4	2	301	315.4
12:00	83	9	1	1	0	1	3	1	99	99.2	58	17	2	1	0	0	0	1	79	80.5
12:15	55	8	2	3	0	0	2	1	71	73.9	65	7	4	6	0	1	0	0	83	93.8
12:30 12:45	55 59	9 10	6	3	0	0	0	0	72 76	77.1 80.3	65 63	8 9	6	0 3	0	1 1	0	0	80 79	84 85.4
H/Total	252	36	13	8	0	1	5	3	318	330.5	251	41	15	10	0	3	0	1	321	343.7
13:00	68	6	0	1	0	0	0	0	75	76.3	58	12	4	0	0	0	0	1	75	76.2
13:15	65	13	2	4	0	0	0	0	84	90.2	67	11	2	3	0	0	2	0	85	88.7
13:30	64	21	3	0	0	0	0	0	88	89.5	60	12	3	2	0	0	1	0	78	81.5
13:45	55	8	5	0	0	2	0	0	70	74.5	61	10	2	3	0	1	0	0	77	82.9
H/Total 14:00	252 55	48 9	10 3	5 2	0	2	0	0	317 72	330.5 77.5	246 56	45 13	11 6	8	0	0	3 0	0	315 78	329.3 84.9
14:15	63	10	3	2	0	0	0	0	78	82.1	59	10	5	2	0	1	2	0	79	83.9
14:30	73	20	3	2	0	0	0	0	98	102.1	110	12	4	2	1	2	0	0	131	138.6
14:45	81	8	4	2	0	0	0	1	96	99.8	102	18	4	1	0	1	2	0	128	131.1
H/Total	272	47	13	8	0	2	1	1	344	361.5	327	53	19	8	1	4	4	0	416	438.5
15:00 15:15	107 92	19 23	3	1 0	0	0	0	0	130 122	132.8 125.9	87 63	16 20	3 2	2	0	0	1 1	1 1	110 88	112.7 88.6
15:15	100	23 14	4	2	2	1 1	1	0	124	131	97	16	4	1	3	0	0	0	121	127.3
15:45	94	26	2	1	0	4	0	0	127	133.3	83	18	5	2	0	1	0	0	109	115.1
H/Total	393	82	12	4	2	8	2	0	503	523	330	70	14	5	3	2	2	2	428	443.7
16:00	99	18	2	2	0	1	0	0	122	126.6	125	31	4	4	1	1	3	1	170	176.6
16:15	103	15	3	2 0	1 1	1 1	1	0	126	131.5 130.9	93	18	5	1 1	1 1	0	0	1	119	123 187.7
16:30 16:45	112 137	13 19	2	2	0	3	1	1	129 165	130.9	148 127	23 21	6 2	1 1	0	2	1	1 3	184 156	156.3
H/Total	451	65	8	6	2	6	3	1	542	559.2	493	93	17	7	2	4	7	6	629	643.6
17:00	148	25	4	4	0	2	0	0	183	192.2	145	21	1	2	1	0	3	1	174	175.5
17:15	142	13	1	1	0	2	3	1	163	164.2	129	20	8	0	0	1	2	3	163	164.4
17:30	130	11	1 .	2	0	1	0	3	148	149.7	140	14	2	3	0	2	2	3	166	169.3
17:45 H/Total	114 534	14 63	7	7	0	5	2 5	2 6	133 627	130.7 636.8	152 566	7 62	5 16	7	1	3	9	8	169 672	172.1 681.3
18:00	102	16	0	2	0	2	2	2	126	127.8	153	17	3	1	0	0	2	1	177	177.8
18:15	112	8	0	1	0	0	1	3	125	123.3	114	10	1	0	1	2	1	3	132	132.5
18:30	99	9	2	2	0	1	0	7	120	119	101	8	0	0	0	0	1	0	110	109.4
18:45	80	3	0	1	0	0	0	1	85	85.5	91	9	1 -	1	0	0	1	3	106	104.8
H/Total	393	36	2	6	0	3	3	13	456	455.6	459	44 671	5	2	1 11	2	5	7	525	524.5
Total	4285	682	146	91	12	42	37	43	5338	5526.7	4269	671	163	85	11	38	40	31	5308	5500.2

Project Name: 07700 Hinckley NRFI
Survey Type: Manual Classified Turning Count

Site No: 18

					Whole 3	Junction				
Time	CAR	LGV	OGV 1	OGV 2	BUS	COACH	MCY	PCY	TOTAL	TOTAL (PCU)
07:00	166	34	6	5	3	7	1	3	225	241.5
07:15	231	47	12	6	2	2	3	1	304	319.2
07:30	283	50	8	2	1	2	2	5	353	357.4
07:45	295	62	7	5	2	5	0	3	379	393.6
H/Total	975	193	33	18	8	16	6	12	1261	1311.7
08:00	315	42	3	1	1	2	3	1	368	371.2
08:15	292	45	10	2	0	1	2	2	354	359.8
08:30	276 266	29	12	3 7	0	0	0	0	320	329.9
08:45	1149	36 152	11 36	13	2	7	1 6	3	326 1368	345 1405.9
H/Total 09:00	223	42	14	4	3	1	3	0	290	304.4
09:00	170	37	9	6	0	1	3	3	229	238.1
09:30	147	30	14	11	0	1	0	0	203	225.3
09:45	163	31	6	11	1	3	0	8	223	237.9
H/Total	703	140	43	32	4	6	6	11	945	1005.7
10:00	143	30	7	8	0	3	2	0	193	208.7
10:15	154	28	6	9	0	1	2	2	202	214.9
10:30	149	33	8	4	0	0	1	0	195	203.6
10:45	140	33	5	6	1	0	2	4	191	197.9
H/Total	586	124	26	27	1	4	7	6	781	825.1
11:00	163	29	8	3	0	2	1	1	207	215.5
11:15	146	26	11	5	0	1	2	0	191	202.8
11:30	169	33	6	2	1	0	1	3	215	218.6
11:45	160	29	10	4	0	1	1	1	206	215.8
H/Total	638	117	35	14	1	4	5	5	819	852.7
12:00	185	32	5	2	0	1	4	3	232	233.3
12:15	144	19	6	9	0	1	3	1	183	196.1
12:30	163	25	11	5	1	1	0	2	208	220.4
12:45	189	27	10	4	0	2	0	1	233	244.4
H/Total	681	103	32	20	1	5	7	7	856	894.2
13:00	164	32	5	1	0	0	0	1	203	206
13:15	168	33	6	7	0	0	3 3	0	217	227.3
13:30 13:45	165 145	41 22	7 8	3 4	0 0	0 3	0	0 1	219 183	224.6 194.4
H/Total	642	128	26	15	0	3	6	2	822	852.3
14:00	151	29	13	7	0	2	1	1	204	220.2
14:15	161	27	11	4	1	1	3	1	209	219.1
14:30	220	40	9	4	1	3	0	1	278	290.9
14:45	216	33	9	3	0	1	4	1	267	273.2
H/Total	748	129	42	18	2	7	8	4	958	1003.4
15:00	231	38	10	3	0	0	1	1	284	291.5
15:15	196	51	7	0	0	4	2	1	261	266.5
15:30	254	34	12	3	6	1	1	0	311	327.3
15:45	211	48	8	4	1	6	0	0	278	294.2
H/Total	892	171	37	10	7	11	4	2	1134	1179.5
16:00	265	54	7	7	1	2	3	1	340	353
16:15	226	40	8	3	2	2	2	1	284	293.9
16:30	306	46	8	1	1	3	6	3	374	377.3
16:45	316	48	4	3	0	4	2	5	382	386.7
H/Total	1113	188	27	14	4	11	13	10	1380	1410.9
17:00	350	51	6	6	1	2	3	2	421	431.4
17:15	318	42 25	9	1	1	4	6	6	387	389.4
17:30	343	35 25	4	5	0	3	2	10	402	404.3
17:45	336	25	8	2	0	0	4	3	378	379.8
H/Total	1347	153	27	14	2	9	15	21	1588	1604.9
18:00	326	40	3	4	0	2	4	4	383	386.1
18:15 18:30	278 248	21 25	2	1 2	1 0	2 1	2 1	8 7	315 287	312.7 285.9
18:30 18:45	248 221	25 15	3 1	2	0	0	1	5	287 245	285.9 243.5
H/Total	1073	101	9	9	1	5	8	24	1230	1228.2
Total	1073	1699	373	204	33	88	91	107	13142	13575
iotai	1034/	1022	3/3	∠∪ 1	J.)	00	31	10/	10147	100/0

Peak	Hours	Totals
07:00	08:00	1261
07:15	08:15	1404
07:30	08:30	1454
07:45	08:45	1421
08:00	09:00	1368
08:15	09:15	1290
08:30	09:30	1165
08:45	09:45	1048
09:00	10:00	945
09:15	10:15	848
09:30	10:30	821
09:45	10:45	813
10:00	11:00	781
10:15	11:15	795
10:30	11:30	784
10:45	11:45	804
11:00	12:00	819
11:00	12:00	819 844
11:15	12:15	836
11:30	12:30	829
11.43	14.43	023
12:00	13:00	856
12:15	13:15	827
12:30	13:30	861
12:45	13:45	872
13:00	14:00	822
13:15		823
13:30	14:30	815
13:45	14:45	874
14.00	15.00	050
14:00	15:00	958
14:15	15:15	1038
14:30	15:30	1090
14:45	15:45	1123
15:00	16:00	1134
15:15	16:15	1190
15:30	16:30	1213
15:45	16:45	1276
16:00	17:00	1380
16:15	17:15	1461
16:30	17:30	1564
16:45	17:45	1592
17:00	18:00	1588
17:15	18:15	1550
17:13	18:30	1478
/.//	±0.00	- 1, 0
17:45	18:45	1363
		1363





Malcolm Ash

From: Rebecca Henson

Sent: 11 November 2019 15:21

To: Luke Hutcheson

Cc: Jonathan Dawes; Harry Sadleir; Anthea Anderson; Alex J Gray; Harry Horsley; Patrick

Brooks; Sonny Tolofari; Gogna, Sunil; Lepidi, Sara;

; Rory McHugh; Vassil Pavlov

Subject: RE: C-07700 Hinckley NRFI Furness Modelling Methodology **Attachments:** 07700-HYD-XX-XX-RP-TP-1021-P02 Furness Methodology.pdf

Luke

Thank you for the attached revised Furness Methodology Technical Note. Apologies for the delay in response. Following review, I can confirm that Option 3 in the attached (Hydrock's preferred approach) is acceptable to Leicestershire County Council.

Kind regards Rebecca

Rebecca Henson

Team Manager
Highway Development Management
Environment and Transport
Leicestershire County Council
Tel:

Mob: Email:

From: Luke Hutcheson

Sent: 29 October 2019 18:45

To: ; Lepidi, Sara ; Gogna, Sunil

Rebecca Henson ; Harry Horsley
; Alex J Gray ; Anthea Anderson

Cc: Jonathan Dawes ; Harry Sadleir ; Rory

McHugh ; Vassil Pavlov

Dear all

Please find attached an updated Furness Methodology Technical Note, updated to offer a third option, and also our recommendations.

As before, this is also saved in the dataroom.

Subject: RE: C-07700 Hinckley NRFI Furness Modelling Methodology

I would be grateful for any comments by the end of the week so that we can close out this item.

Kind regards

Luke

Luke Hutcheson BSc (Hons) MSc MCIHT

Senior Consultant | Transportation

Hydrock



From: Luke Hutcheson
Sent: 09 August 2019 18:10

To: Lepidi, Sara ; Sonny Tolofari ; Harry Horsley

Cc: Jonathan Dawes
Gogna, Sunil ; Harry Sadleir
; Rory McHugh
HE instructions ; Vassil Pavlov

Subject: RE: C-07700 Hinckley NRFI Furness Modelling Methodology

Hi all

Please find attached the Furness Methodology Note, also saved into the Dataroom.

The note remains in draft, awaiting the resolution of the discussion below, as the conclusions drawn from this discussion will provide confirmation of the methodology and approach.

The note should therefore aid the discussion of below, and should not detract from the importance of discussing and resolving the discrepancies.

Monday 12th will be three weeks since the discrepancies from the spot checks were presented, and so I hope this can be treated with some urgency.

Many thanks

Luke

Luke Hutcheson BSc (Hons) MSc MCIHT

Senior Consultant | Transportation

Hydrock

Merchants' House North, Wapping Road, Bristol BS1 4RW Tel: Internal Ext: Mob:

Sent: 08 August 2019 11:47

To: Vassil Pavlov ; Sonny Tolofari ; Harry Horsley

Cc: Jonathan Dawes ; Harry Sadleir

Gogna, Sunil ; Reby ; Laura P Shepherd

; Rory McHugh ; Mark Pearce ; HE instructions

Subject: RE: C-07700 Hinckley NRFI Furness Modelling Methodology

Hi Vassil,

Thank you for providing the information regarding the comparison exercise that you have undertaken between PRTM and traffic survey flows and regarding the Furness methodology to match the two datasets.

Having reviewed your email below and the attached spreadsheet titled "07700-HYD-XX-XX-CA-TP-0022-P01.04 Furness Analysis", we consider some of the discrepancies between the 2036 WoDWoS PRTM flows and the interpolated and factored 2018 base flows to be significant. We recommend this is further investigated to exclude the possibility of this being related to PRTM validation issues in the study area.

Notwithstanding the above, based on our previous experience with similar techniques, we would consider the first methodology presented (derive target trip ends directly from the PRTM without interpolation) to be a more suitable approach as this would reduce the amount of assumptions applied to derive the target flows. Also, the flow assignment in these forecasts would fully take into account the available capacity within the network, ensuring that no unrealistic volume are being assigned.

However, as it is our understanding that a Furness Methodology Technical Note (TN) is currently being prepared and will be shortly issued for review, we will only be in a position to confirm our preferred approach following the review of this document. In order to help us to take an inform decision, please ensure that the forthcoming TN clearly sets out the two different methodologies and pros / cons for each of them.

Please also note that for Highways England the 2036 scenario is for information only. Therefore, we would request the TN to also consider opening year (2026) flow forecasts.

We look forward receiving the additional information and the meantime we hope you find this advice useful.

Kind regards, Sara

Sara Lepidi

Senior Consultant, Transportation & Traffic

AECOM

The Colmore Building
Colmore Circus Queensway
Birmingham, B4 6AT, United Kingdom
T +44(0)121-262-1900

Built to deliver a better world

LinkedIn Twitter Facebook Instagram



From: Vassil Pavlov

Sent: 29 July 2019 11:52

To: Sonny Tolofari Rebecca Henson

; Harry Horsley

Cc: Jonathan Dawes

Gogna, Sunil ; Lepidi, Sara ; Rory McHugh

; Luke Hutcheson ; Mark Pearce

Subject: FW: C-07700 Hinckley NRFI Furness Modelling Methodology

Good morning all,

Further to my last email, I was wondering if you have had a chance to review the attached and offer your views. As discussed before, we are keen to agree on a final methodology as soon as possible in order to proceed with the subsequent stages of the wider modelling exercise.

We would therefore appreciate any comments/input you are able to provide.

I look forward to hearing from you.

Many thanks

Kind regards

Vassil Pavlov BEng (Hons) GradCIHT MTPS

Graduate Consultant | Transportation

Hydrock

Northern Assurance Buildings, 9-21 Princess St, Albert Square, Manchester M2 4DN



```
From: Vassil Pavlov

Sent: 22 July 2019 17:19

To: Sonny Tolofari ; Rebecca Henson
; Harry Horsley

Cc: Jonathan Dawes ; Harry Sadleir
Gogna, Sunil ; Lepidi, Sara ; Rory McHugh
; Luke Hutcheson ; Luke Hutcheson
```

Subject: C-07700 Hinckley NRFI Furness Modelling Methodology

Dear all

As discussed at the latest highways workshop, please see below and attached our comparison of the PRTM/traffic survey flows, with Furness applied. This technique has been discussed/agreed with the modelling team and is consistent with the advice given to date.

As you may recall, we discovered potential discrepancies between the 2036 WoDWoS PRTM flows and the interpolated and factored 2018 base flows during the Furness procedure at Site 18 - New Rd / Long St / Broughton Road roundabout junction, the survey for which was undertaken on 26/06/2018.

To ascertain the extent of these discrepancies across the rest of the network, we have undertaken spot checks at further four junctions, namely:

- Site 21 Coventry Road / B581 Broughton Road (Survey undertaken on 26/06/2018)
- Site 22 M69 J1 / A5 (Survey undertaken on 10/04/2019)
- Site 28 B4669 Leicester Road Sapcote / B4114 Coventry Road (Survey undertaken on 26/06/2018)
- Site 29 The Common Barwell / A47 / B4668 Leicester Road (Survey undertaken on 26/06/2018)

This provides a mixture of junction types and locations. The location of all five junctions is illustrated below.



The spot checks involved comparing the observed base flows with those predicted by the model for the same year (derived through linear interpolation). The GEH statistic was then calculated to provide an indication of the statistical significance of the differences. The results of this is summarised in the table below, with the full calculations attached. Negative flows mean that the observed (surveyed) flows are lower than the PRTM forecast.

Arm	Site 18 - N Long St / B Roa	roughton	Site 21 - (Road / Broug	B581	Site 22 - M	69 J1 / A5	Site 28 - Leiceste Sapcote Coventi	er Road / B4114	Site 29 - The Common Barwell / A47 / B4668 Leicester Road		
		GEH		GEH		GEH		GEH		GEH	
AM	Difference	Statistic	Difference	Statistic	Difference	Statistic	Difference	Statistic	Difference	Statistic	
From A	+256	17	-349	13	+70	2	-49	2	-72	4	
From B	-125	7	+380	16	+90	4	-135	7	-166	4	
From C	-44	4	-93	4	+33	1	+19	1	+46	2	
From D	-66	3	-4	0	-285	13			0	0	
From E					-96	4					
From F					+40	1					
PM											
From A	+34	2	+192	7	-114	5	+5	0	-95	6	
From B	+157	8	+116	5	-6	0	+313	16	+134	4	
From C	-187	10	+421	18	+80	3	+132	9	-18	1	
From D	+3	0	+110	7	-237	11			-97	3	
From E					-222	6					
From F					+251	8					
AM											
From A	+106	8	+15	1	-134	6	-137	6	-20	1	
From B	+34	2	+58	2	-271	10	-100	5	-31	1	
From C	-18	1	+31	1	+69	3	+73	6	-117	4	
From D	-101	4	-170	9	+161	7			-25	1	
From E					-232	7					
From F					+261	8					
PM											
From A	-46	2	+271	11	+64	2	+395	17	+64	3	
From B	+57	3	+189	7	-142	6	+19	1	-229	6	
From C	+30	2	+76	4	+273	9	+36	3	-64	3	
From D	-34	1	+269	14	-113	5			+154	6	

From E			-124	5		
From F			-205	6		

The difference was also gauged for forecast trip ends for 2036 for the two variations of the Furness procedure. This is contained within the comparison tab of the attached spreadsheet for each junction.

Taking the above into consideration, we have the following questions.

- Do you consider the methodology shown to be acceptable/ in accordance with the advice you have given us to date?
- Do you consider the differences in flows to be significant/acceptable?
- Can the dates of the surveys be reviewed by LCC to check against road space bookings/diversions at that time, that might be skewing the results?

We welcome any further thoughts/opinions.

Many thanks

Kind regards

Vassil Pavlov BEng (Hons) GradCIHT MTPS

Graduate Consultant | Transportation

Hydrock

Northern Assurance Buildings, 9-21 Princess St, Albert Square, Manchester M2 4DN

Tel: Internal Ext: Email:

hydrock.com



Five consecutive years in the top 40 'Sunday Times 100 Best Companies to Work For' listing, and winner of the NCE100 'Health and Wellbeing Leader of the Year' award, 2019.



Hydrock Consultants Limited, company number 3118932 and Hydrock NMC Limited, company number 05579646, are subsidiaries of Hydrock Group Limited, company number 6644687, registered in England and Wales at Over Court Barns, Over Lane, Almondsbury, Bristol, BS32 4DF.

Before printing this e-mail, please think about the environment.

Disclaimer: The information in this e-mail is confidential and may be read, copied or used only by the intended recipients. If you are not the intended recipient you are hereby notified that any perusal, use, distribution, copying or disclosure is strictly prohibited. If you have received this e-mail in error please advise us immediately by return e-mail at bristol@hydrock.com and delete the e-mail document without making a copy. Whilst every effort has been made to ensure this email is virus free, no responsibility is accepted for loss or damage arising from viruses or changes made to this message after it was sent.

This e-mail and any files transmitted with it are confidential. If you are not the intended recipient, any reading, printing, storage, disclosure, copying or any other action taken in respect of this e-mail is prohibited and may be unlawful. If you are not the intended recipient, please notify the sender immediately by using the reply function and then permanently delete what you have received.

Incoming and outgoing e-mail messages are routinely monitored for compliance with Leicestershire County Council's policy on the use of electronic communications. The contents of e-mails may have to be disclosed for requests under Data Protection or Freedom of Information legislation. Details about how we handle information can be found at https://www.leicestershire.gov.uk/data-protection

The views expressed by the author may not necessarily reflect the views or policies of the Leicestershire County Council.

Attachments to e-mail messages may contain viruses that may damage your system. Whilst Leicestershire County Council has taken every reasonable precaution to minimise this risk, we cannot accept any liability for any damage which you sustain as a result of these factors. You are advised to carry out your own virus checks before opening any attachment.



